

126

MIDDLEFIELD HUNTSBURG

Sec. B & C

Transit Book

CLAY ST. Transit Notes.

FIELD BOOK

740

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER

TABLE FOR REDUCING PERCHES TO FEET AND INCHES.

PERCH	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.
1	16.6 in.	21	3.46 6 in.	41	6.76 6 in.	61	10.06 6 in.	81	13.36 6 in.		
2	33.0	22	3.63 0	42	6.93 0	62	10.23 0	82	13.53 0		
3	49.6	23	3.79 6	43	7.09 6	63	10.39 6	83	13.69 6		
4	66.0	24	3.96 0	44	7.26 0	64	10.56 0	84	13.86 0		
5	82.6	25	4.12 6	45	7.42 6	65	10.72 6	85	14.02 6		
6	99.0	26	4.29 0	46	7.59 0	66	10.89 0	86	14.19 0		
7	1.15 6	27	4.45 6	47	7.75 6	67	11.05 6	87	14.35 6		
8	1.32 0	28	4.62 0	48	7.92 0	68	11.22 0	88	14.52 0		
9	1.48 6	29	4.78 6	49	8.08 6	69	11.38 6	89	14.68 6		
10	1.65 0	30	4.95 0	50	8.25 0	70	11.55 0	90	14.85 0		
11	1.81 6	31	5.11 6	51	8.41 6	71	11.71 6	91	15.01 6		
12	1.98 0	32	5.28 0	52	8.58 0	72	11.88 0	92	15.18 0		
13	2.14 6	33	5.44 6	53	8.74 6	73	12.04 6	93	15.34 6		
14	2.31 0	34	5.61 0	54	8.91 0	74	12.21 0	94	15.51 0		
15	2.47 6	35	5.77 6	55	9.07 6	75	12.37 6	95	15.67 6		
16	2.64 0	36	5.94 0	56	9.24 0	76	12.54 0	96	15.84 0		
17	2.80 6	37	6.10 6	57	9.40 6	77	12.70 6	97	16.00 6		
18	2.97 0	38	6.27 0	58	9.57 0	78	12.87 0	98	16.17 0		
19	3.13 6	39	6.43 6	59	9.73 6	79	13.03 6	99	16.33 6		
20	3.30 0	40	6.60 0	60	9.90 0	80	13.20 0	100	16.50 0		

COURT HOUSE
CHARLTON
PHONE 250-X

B. K. ELLIOTT COMPANY, PITTSBURG, PA.

DRAWING MATERIALS AND SURVEYING INSTRUMENTS

Huntsburg N. & S. Center Road.
& Clay St.

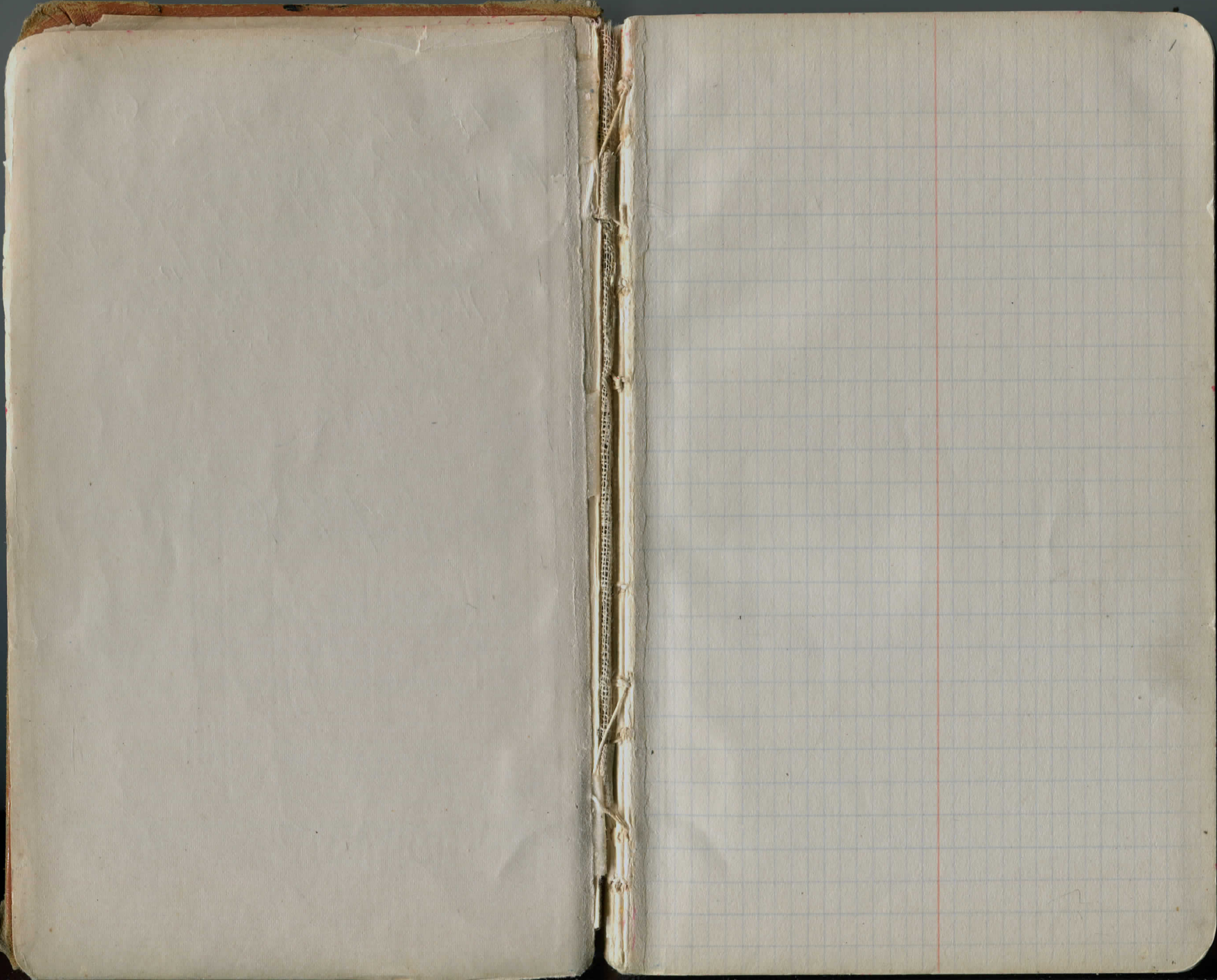
Madison Rd (Route 528)
thru Huntsburg Twp

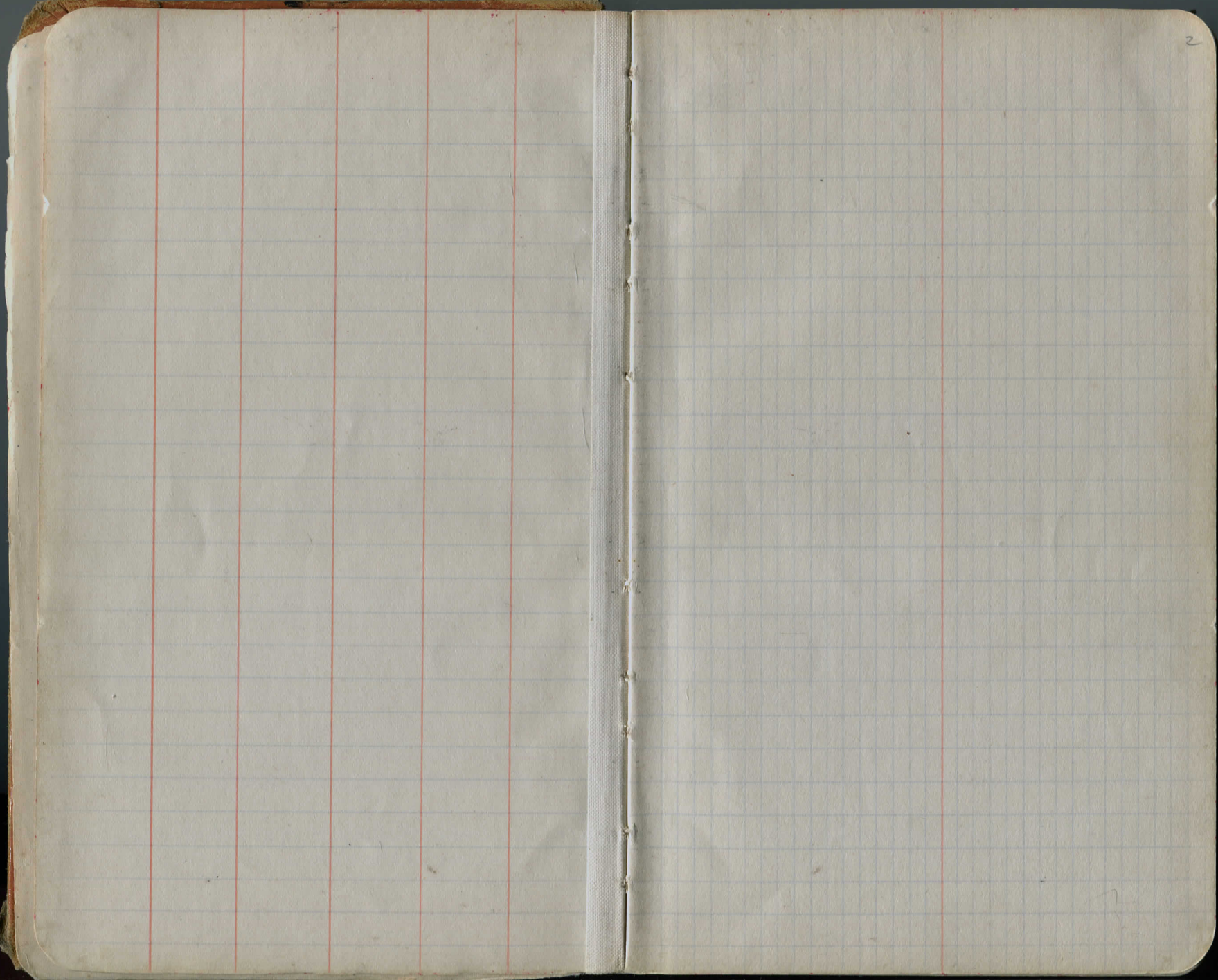
Pg 55 (Pg 58 1952)
Pg 1-52
72-

Note:

SEE FB 313 FOR 1975-76 WORK
(CHARLTON-WINDSOR ± 1000' N E S)

(126)





TB 126
TRANSIT NOTES

Sta Angle Bearing Sec B

10

+53⁵ 0°-0'

9

8

7

6

5

4

3

2

1

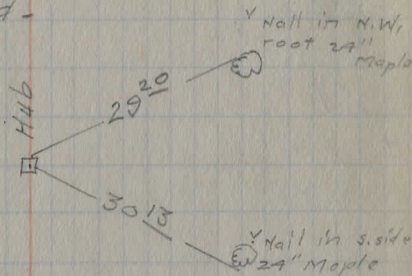
0

P.M. 3-14-21
12-18" mud

M¹FIELD-HUNTSBURGE

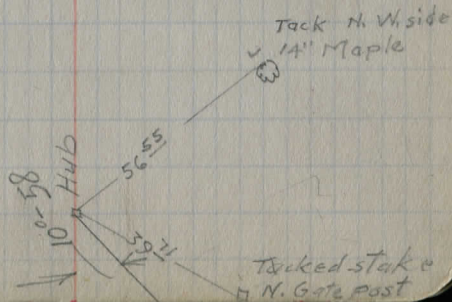
Hanna T.
Grau c.
Thrasher c.
3

Note: - All stakes set on 25' offset to Rt. Unless noted.



{Note - Little Transit in }
{very bad adjustment. }

Town Line (Approx.)



Sta. Angle Bearing

22

21

20

19

+93[⊥] 0°-0'

17

16

15

14

13

12

11

(Mag.)

E.

30'

3°

⊥

Staple in S side
15" Maple



35.92

HUB

Staple in S.E.
side 10" Maple



30.85

HUB

⊥

Fair
Warm
Mud-

Sta. Angle Bearing

32

3-15-'21

+294[±] Δ 0°-29' Rt.

31 Not set

+90

30

29

28

27

26

25

24

+88¹ Δ 0°-0'

23

NE root
Nail in N.
side 15"
Maple

~~37³²~~
36³⁰

1-07
1294

~~38³²~~
38³²

S&W
Nail in
Y side
24" Maple

Nail N.E. side
24" Apple

28¹²

Hub

Nail S.E. side
12" Maple

10⁶⁵

Sta. Angle Bearing

44

43

42

41

40

39

+94^g Δ 0°-0'

38

37

36

35

34

33

Nail in N. side
12" Maple



36.74'

150°

44.75'

M.H.
Tacks in
S.W. cor. Bld.
Milk House

Sta Angle Bearing

56

55

54

53

52

51

50

+892 Δ 0°-22' Lt.

49

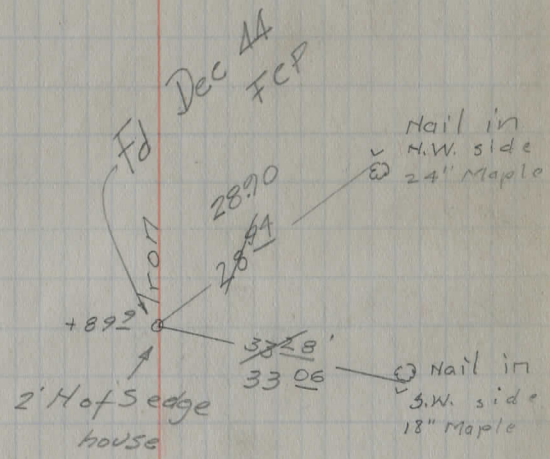
48

47

46

45

H. 3° - 30' E-



47+47 P.L. P.L.

Sta. Angle Bearing

68

67

66

65

64

63

62

61

+44^E Δ 0°-0'

60

59

58

57

I.P. Fd Dec 44
Hush

+44^E

Hub

35 50

Gone

Nail in N.W. side
6" Maple
End Map

26 58'

Nail in S.W. side
14" Maple

42 45

Spk. SW Side
12" Maple

30' from
N end

Sta Angle Bearing

79

78

+28⁸ Δ 0°-0'

77

76

75

74

73 —

72

71

70

+06^A Δ 0°-0'

69

Nail in N.
side 24"
Apple

41.93'

Nail in E.
root 18"
Apple

38.50'

73 ± 20 = $\frac{1}{2}$ HELL RD.
35' Offset to Rt.

Nail in N.E.
side 18" Maple

34.53'

Nail in S.E. side
18" Maple

37.00'

H

Sta. Angle Bearing
 $+28^{\circ} \Delta 0^{\circ} - 0'$

91

90

89

88

87

86

85

84

83

82

81

80

~~E~~

Hub

38.40'

10
 Nail in N.W.
 side 24"
 Hedge Apple

38.58'

Nail in S.W.
 side 18" Hedge
 Apple

Sta. Angle Bearing

104

103

102

101

100

99

98

97

96

95

94

93

92

Sta. Angle Bearing
114

113

+33^E Δ 0°-0'

112

111

110

109

108

107

106

105

+30^A Δ 0°-0'

Iron

32 33'

44 40'

30'
Nail in N. side
15" Maple

30'
Nail in S.W. side
12" Maple

30'

30'

30'

30'

25'

Nail in N.E. side
18" Walnut

41 35

40 34

Hub

Nail in S.E. side
18" Walnut

Sta. Angle Bearing

126

125

124

123

+24°. 0'-0'

122

121

120

119

118

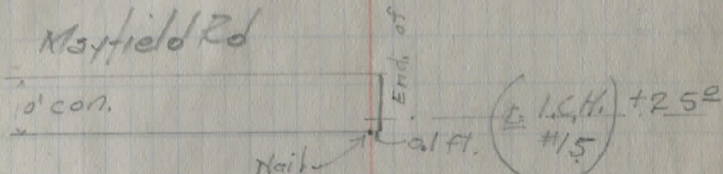
117

116

115

13

25



25

25

25

25

25

30'

Sta. Angle Bearing

138

137⁶

136⁵

135⁴

134³

133²

+ 94.6
0° 0'

132¹

131⁰

130⁹

129⁸

128⁷

127

L

R

Rt

14

25'

30'

25'

Nail in N.E.
side 12"

Maple

3705

3020

H46

+ 94.6

Nail in
S.E. side
12" Maple

4283

432

I.P.F.D 1-25-17

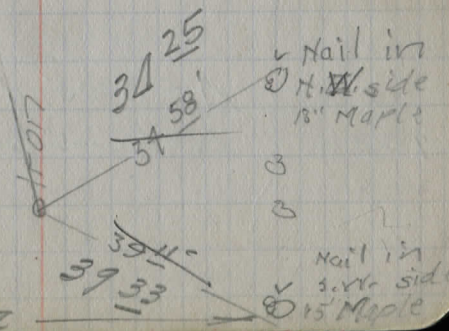
Sta. Angle Bearing

Continued on page 17

7
 $130 + 69'$ Δ $0^{\circ}03'20''$ Left
 End of survey

I.P. Fd
 1-25-47

SE side



Oct. 23, 1923
Cold, Windy.

Marks
Grau

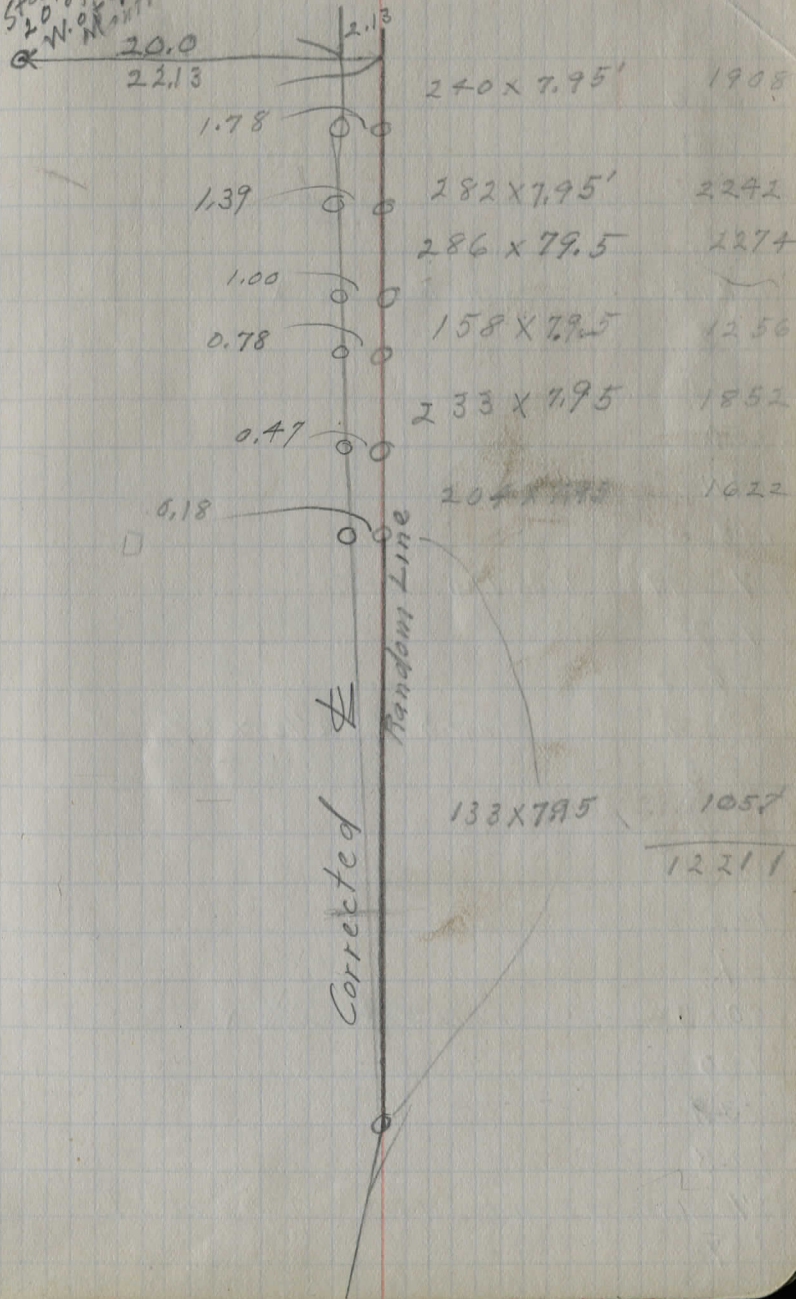
Sta. Angle Bearing

137 + 69.11

$\Delta = 0^{\circ}03'20''$ Left, Corrected \neq

$\Delta = 0^{\circ}02'45''$ Left, Random Line

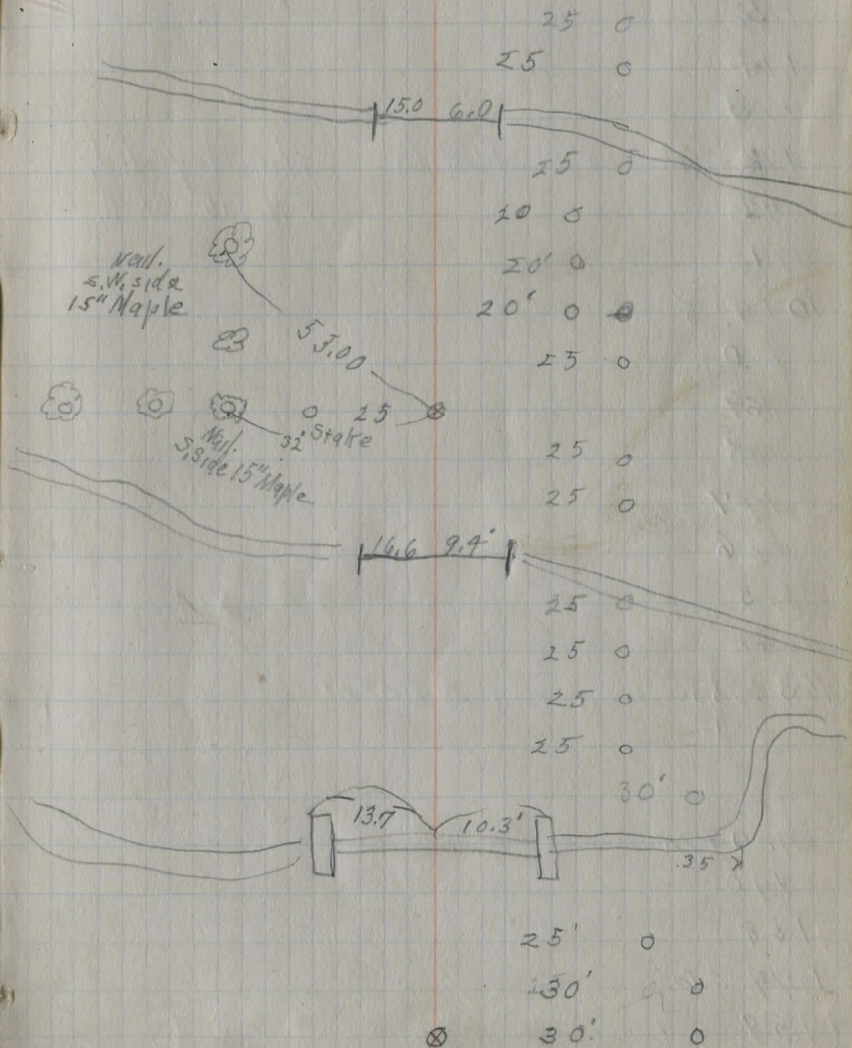
Stake
20' offset
W. of
Newville Rd.



- 156
 155
 154
 153
 152+85 Stone Box 2 1/2 X
 152
 151
 150
 149
 148
 147+89.1 Iron Pin $\Delta = 0^{\circ}0'$
 147
 146
 +55 Stone box 2 1/2 X 2 1/2
 145
 144
 143
 142
 141
 140+38 Stone Box 2 1/2 X
 140
 139
 138
 137+69.11 Iron Pin $\Delta = 0^{\circ}03'20''$ L
 137

Stakes offset 25' Right unless
 otherwise indicated

Oct. 26, 1923 Fidler
 Cool - Cloudy Marks
 Gray.

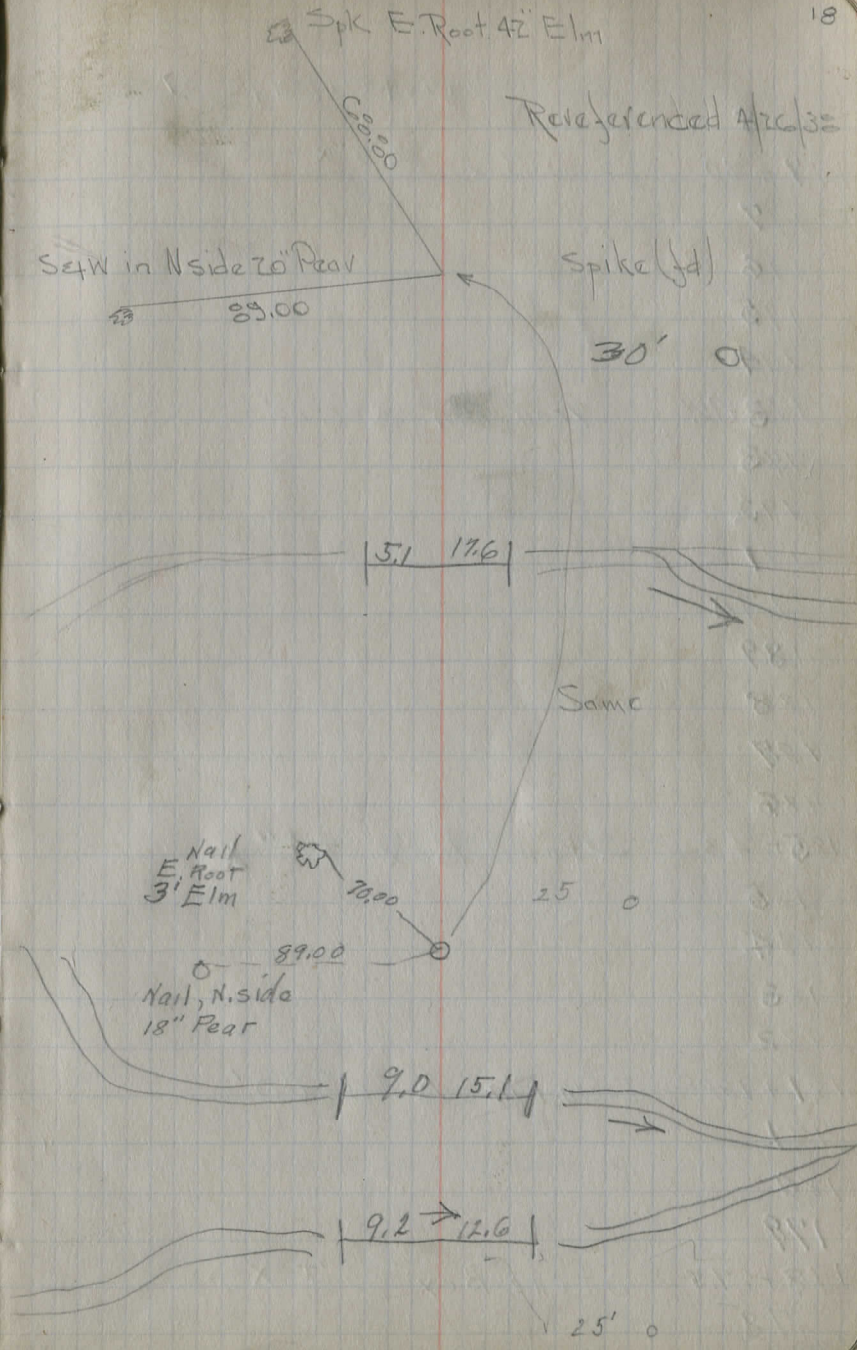


179
176
175
174
173
172+74.7
172
171
170+06.5
170
169
168
167
166
165
164

163+55.55 Iron Pin $\Delta = 0^{\circ}0'$

160+78
160
159
158+40
158
157

Cross Roads Hantley Rd.
TH 115 SAM.



Continued on page 37

198
197+80 Stone Box 2'3" X

197

196

195

194

193+968 Iron Pin $\Delta = 0^{\circ}00'$

193

192

191

190

189

188

187

186

185+43 Stone Box ~~2'4" X~~

185

184

183

182

181+98⁰⁰ Iron Pin $\Delta = 0^{\circ}00'$

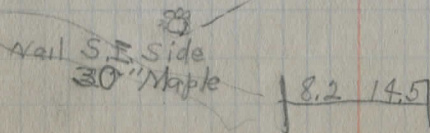
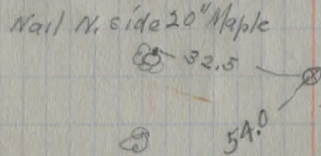
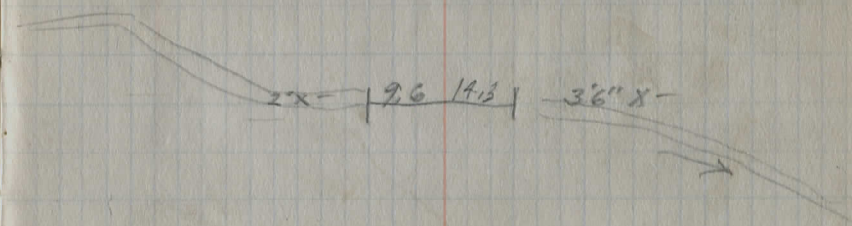
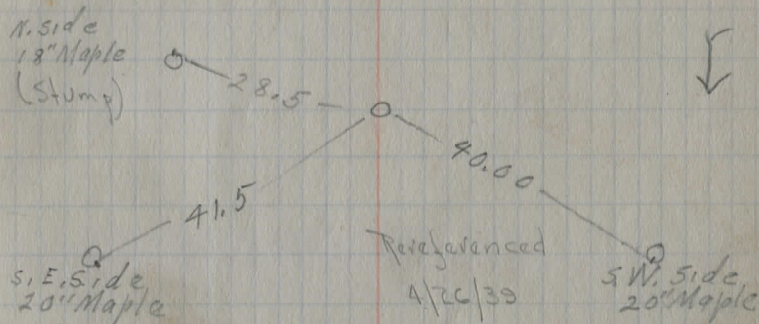
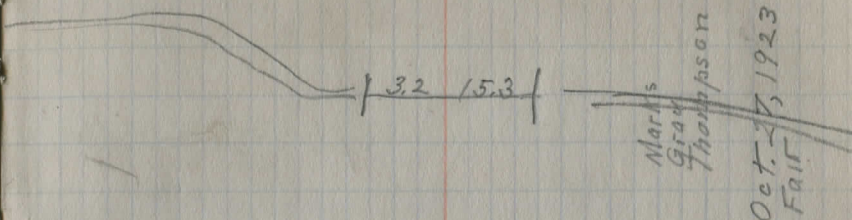
181

180

179

178+67.5 Stone Box 2'± X

178



TOPOGRAPHY

20

07

+85 15' ③

+31 13' †

+06 27' ③

06

+82 26' ③

+60 27' ③

+32 27' ③

+5
+25 26' ③

+05 26' ③

04

+85 27' ③

+35 12' †

03

+60 29' ③

+50 27' ③

02

+75 27' ③

③ 20'

+60

01

+88 28' ③

+90?

+45 28' ③

+40 11 †

+20
0

Jim Ishe

Barnes

Miller



pt.

③ 35'

80'

+63 14 ^{22'} +

+05 13' +

⊙14

+95

⊙ 24'

⊙
⊙

⊙13

+95 ^{22'} +

⊙ 15'

+10

+04 23' ⊙

⊙12

+33 23' ⊙

⊙11

+80 23' ⊙

+67 13' +

+60 27' ⊙

+40 27' ⊙

+15 27' ⊙

⊙10

+90 27' ⊙

⊙ 35'

+65 27' ⊙

+43

⊙ 22'

+40 27' ⊙

80'

+30

+20

⊙9

+75 50'

+11 12' +

⊙8

I

G

000 25' +40 24' 0
 0 023
 0 25' +65
 P.L. +45 24' +57 13 +
 +75
 +15 4' 0

0 12' 022
 021
 +75 25 0
 +66 13' +
 +50
 +30
 020
 019
 +66 13 +
 29' +53
 0 018
 0 +75
 0 30' +12
 017
 +48
 +46 22 0
 016 14 +
 015 22 0

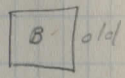
P.L.

			30'	See
		Q ₃₃		
		+85	19'	+
				800
		Q ₃₂		
		+95		3
⊖	25'	+52	30	⊖
		+22		
		+12		
		Q ₃₁		
		+87	17'	+
		Q ₃₀		
⊖	25'	+50		
		Q ₂₉		
		+92	16'	+
⊖	25'	+70		
		+30	19'	⊖
		+25	10'	⊖
		Q ₂₈		
		Q ₂₇		
⊖	20'	+75		
		+72	14'	+
⊖	27'	+10		
		Q ₂₆	17'	
⊖	27'	+85		
		Q ₂₅		
⊖	20'	+50		
		+44	15'	+
⊖	23'	Q ₂₄		

Rd (Approx) Rd. (Approx)
 (Approx)

000000

+53 19' + 0 0 0
 044
 +75
 +20 =
 047 31'
 +92
 +72 19' +
 +50 20 0
 +10 30 0
 042
 +10 041



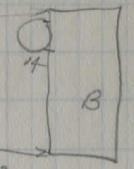
0 30'

+90 20' +
 040
 +27 32' M.H.
 +20 =
 +10
 039
 +95 20' +
 +85



80'

+35
 +35
 038
 +46 = 40'
 +60 30' 0 0
 +50
 037



G. Bauer

0 0 30'

+95 20' +
 +30 30 0
 034
 +95 30 0
 +05 30' 0
 035
 +90 20' + 0 0
 30' 0 0
 03A

G. Bauer

000

+62 15'

053

000000

100

+65

052

+80 15'

000

000000

0/00

051

+60

+36

+04 15'

050

+90

000

000000

H

27'

00000

34

049

+23 16'

048

000

000000

PL1

+47

+39

+25

047

+37

046

23

20

18'

27'

PL1

000

000

000000

0000

32

045

0000

30 30 062
 +95
 +50 18 +
~~+55~~ 267

061
 26' 00000

060
 +70 14' + 00000

059 00000

0
 0
 0
 0
 0
 DM 31'

31' 058
 +91 14' + 00000

057 24 0
 +75 = 000

056 65' H

0
 0
 0

+53 10' + 000
 +05 100
 055

05A 00000

B

+90 21'
+60 11' +
+50 21' 3
⊙72

⊙ 29' +60 21'
⊙

⊙71

⊙ 29' +77 10' +
⊙

⊙70

⊙
⊙

+41 21'

+03 12' +

⊙69 12' + 60' 3

+95
+85

⊙ 29' +50 22' ⊙

⊙ +30 22 ⊙

⊙ 29' ⊙68

+09 12' +

⊙67

⊙66

⊙ 30 +70

+20 13 +

⊙65

+94

⊙ 30 +50

⊙64

+35 15' +

⊙63



PL

25 +10 +05 18' + 26'

25 +50
~~25~~

81

+12 17' +

80 25'

79

+27 16' +

78 23'

+46

77

+80

+60

+50 14' +

76 20'

+20

75

+85 23' 8

+75 40'

+50 16' +

+35 25' 8

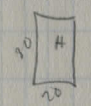
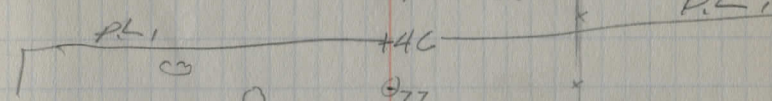
74

+45 23'

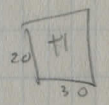
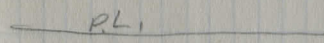
+65 13' +300

+20 30'

93 Rd (approx)

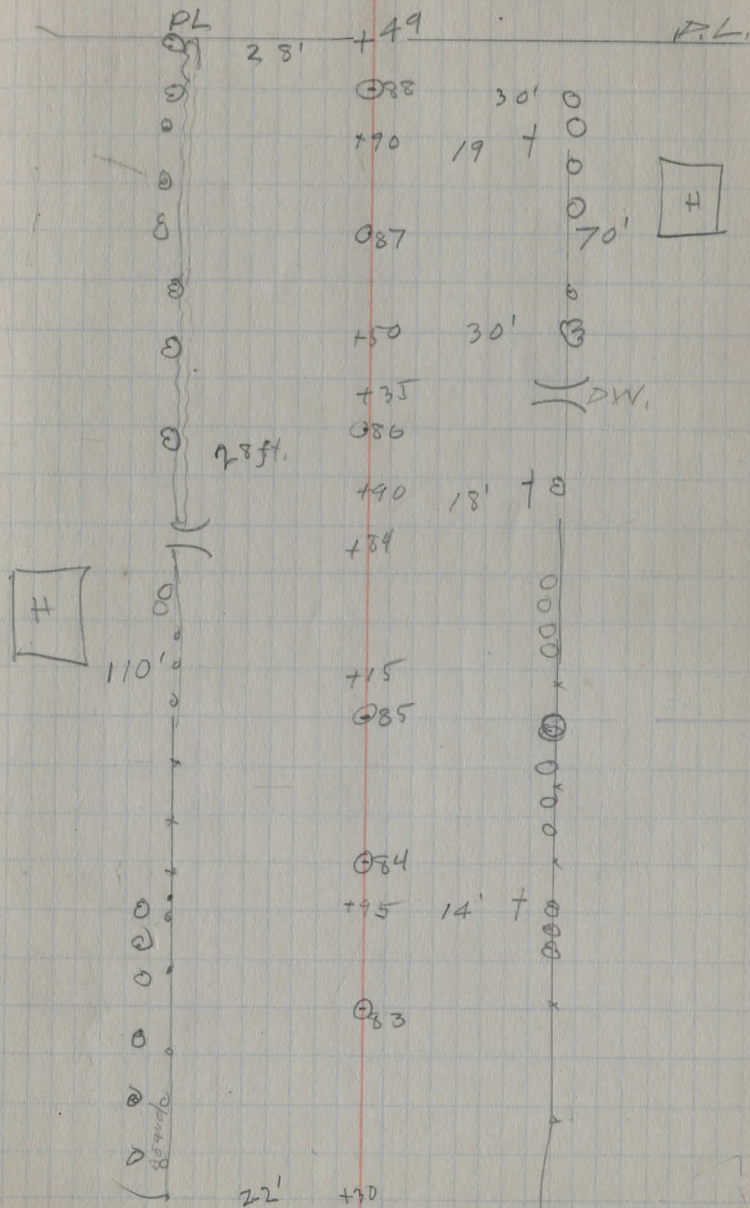


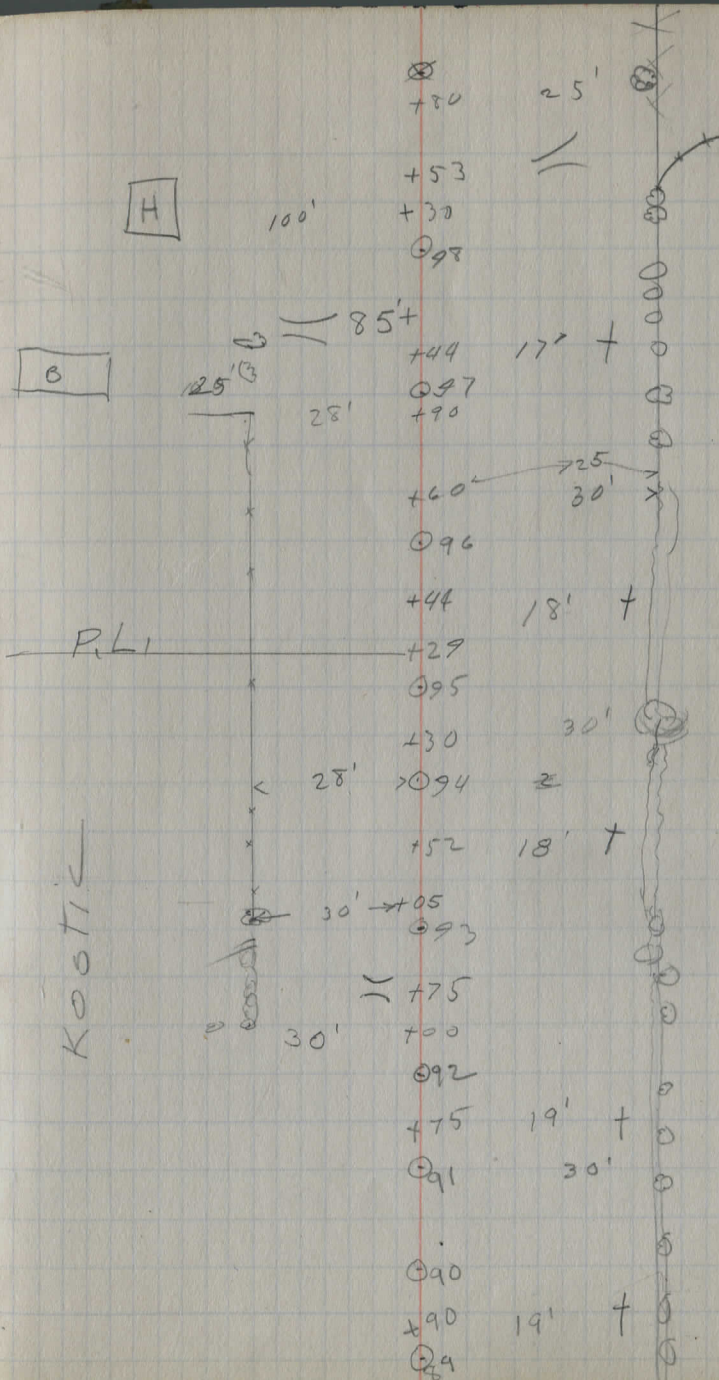
70 100



Cem- Road 30'

R. 1st ce





+55 20' +
 +30 30'
 @107

+01
 @106

+40 19' +

@105

@ 30' +60
 @ 30' +10
 @104

25' +60 22' @
 27' +51

x x

x
 @ 25' +25 18' +
 @103

x @
 @ 25' +60
 +30
 @102

@ 30' +60
 @ 25' +33 18' + @

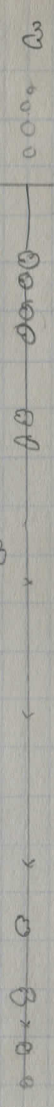
@ 30'

@101
 +75

+38 30

@100
 +40
 +30 25'
 25'

+50 18' +
 +25 150
 @9

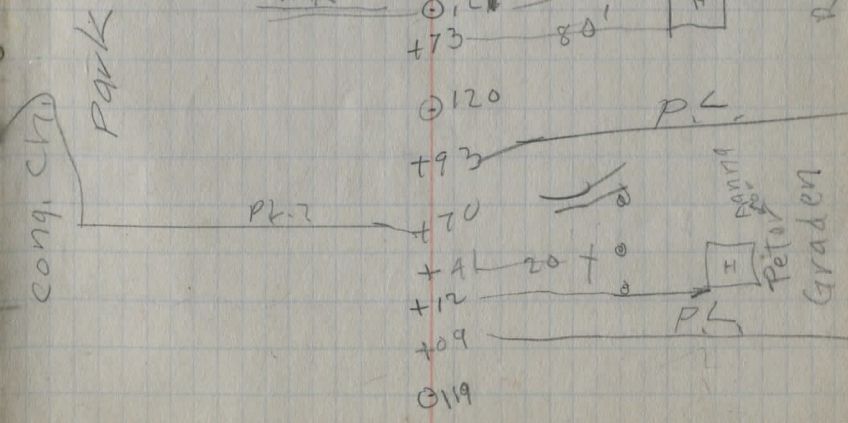
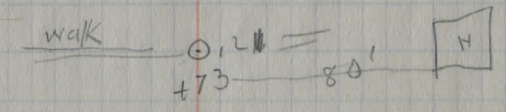
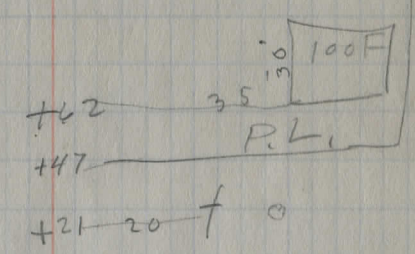
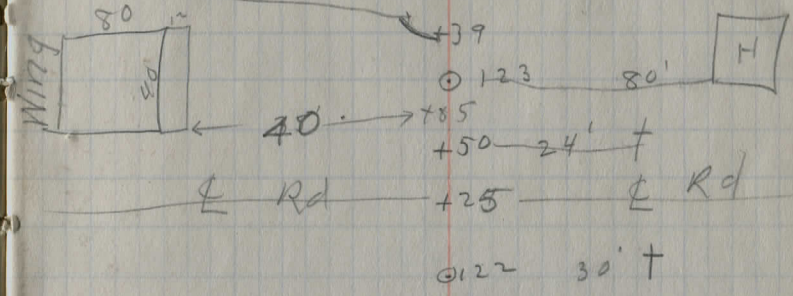
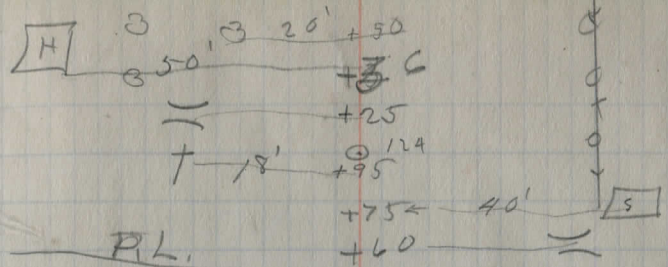


P.L.

Bartholomew-

O.L. Strong-

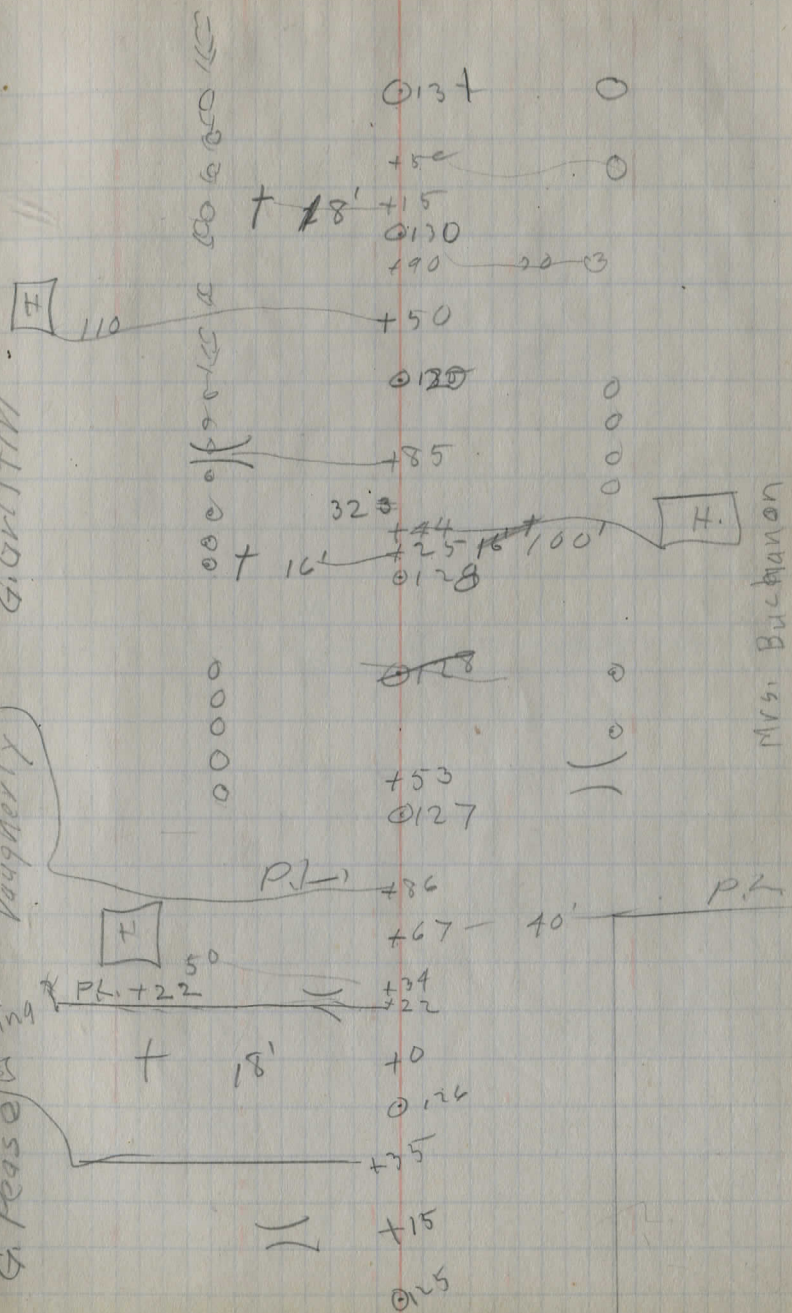




G.V. McClintock 84

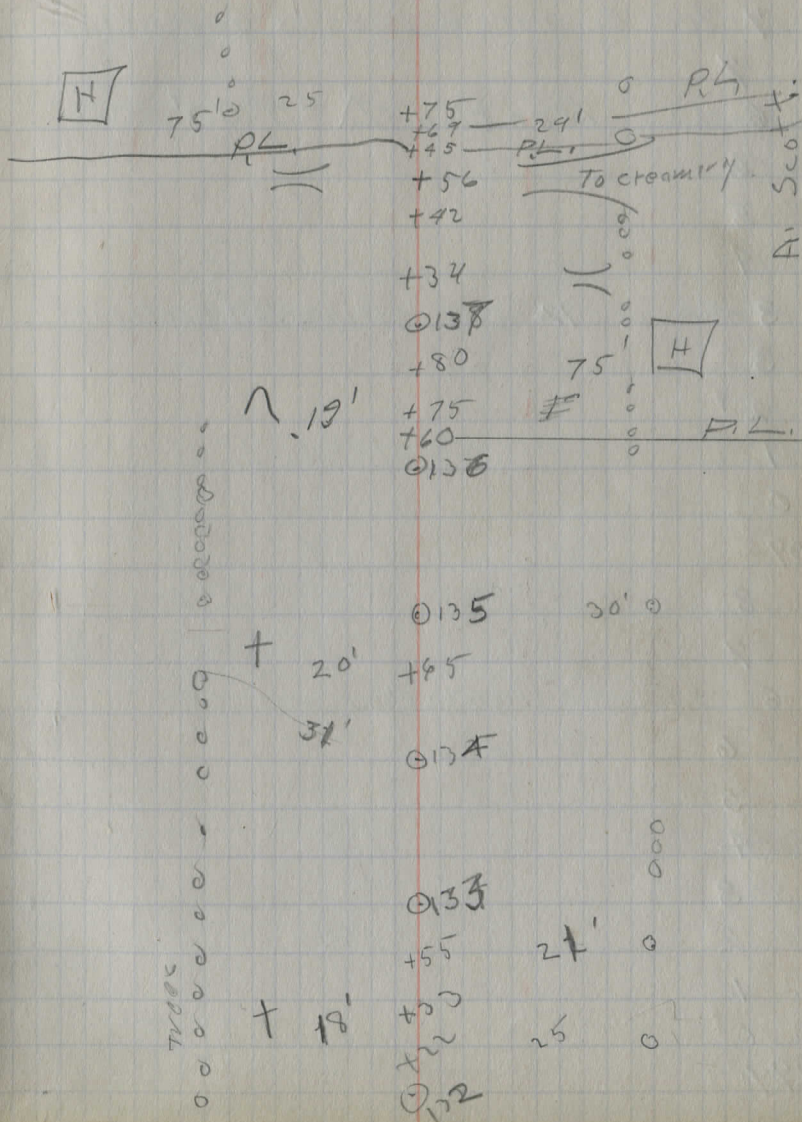
R.W. McClintock

G. Pease
Paugherty
G. Griffith



Mrs. Buchanan

Willbee

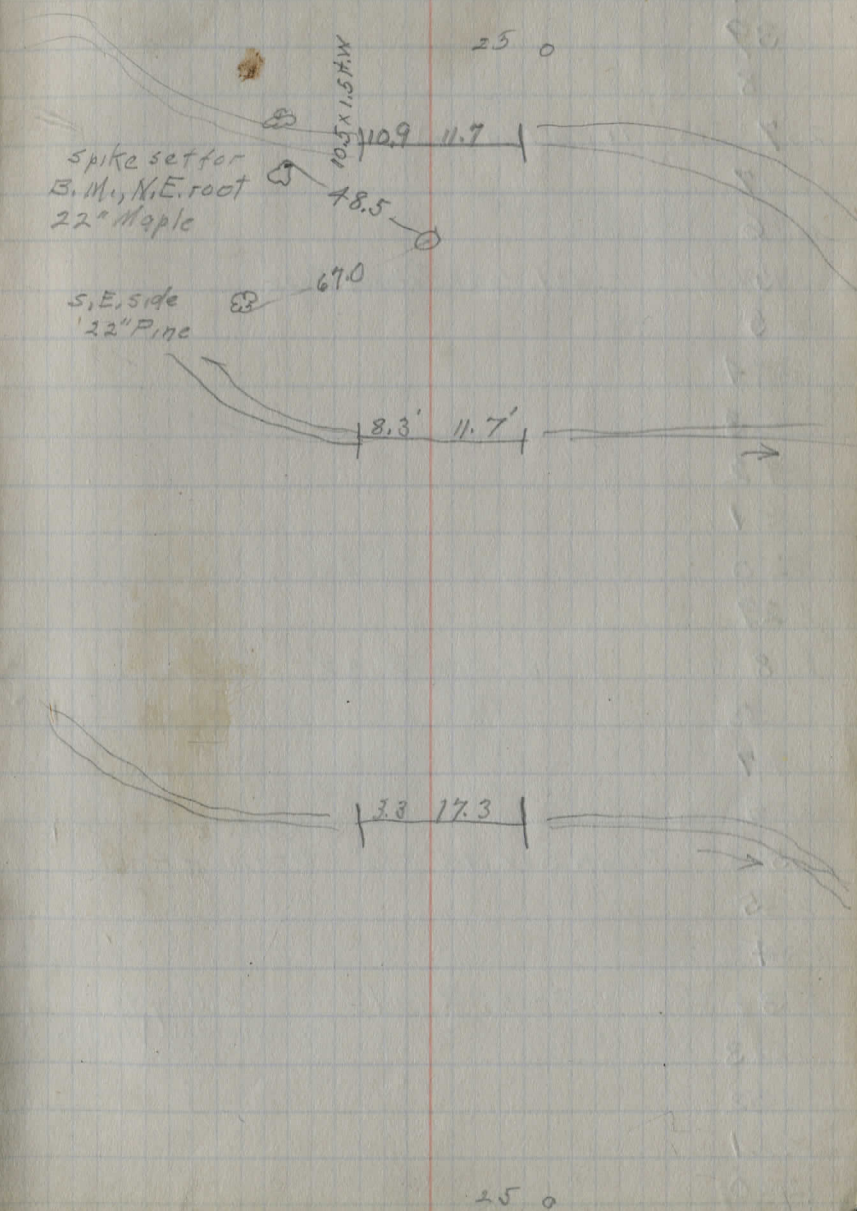


219
 218
 217+70 Concrete Box 34" x Good condition
 217
 216+08.3 Iron Pin $\Delta = 0^{\circ}00'$
 216
 215
 214
 213+07.6 12" Iron Pipe, C.I. Sectional
 213
 212
 211
 210
 209
 208
 207
 206+05.5 3' X 3' Stone Box
 206
 205
 204
 203
 202
 201
 200
 199

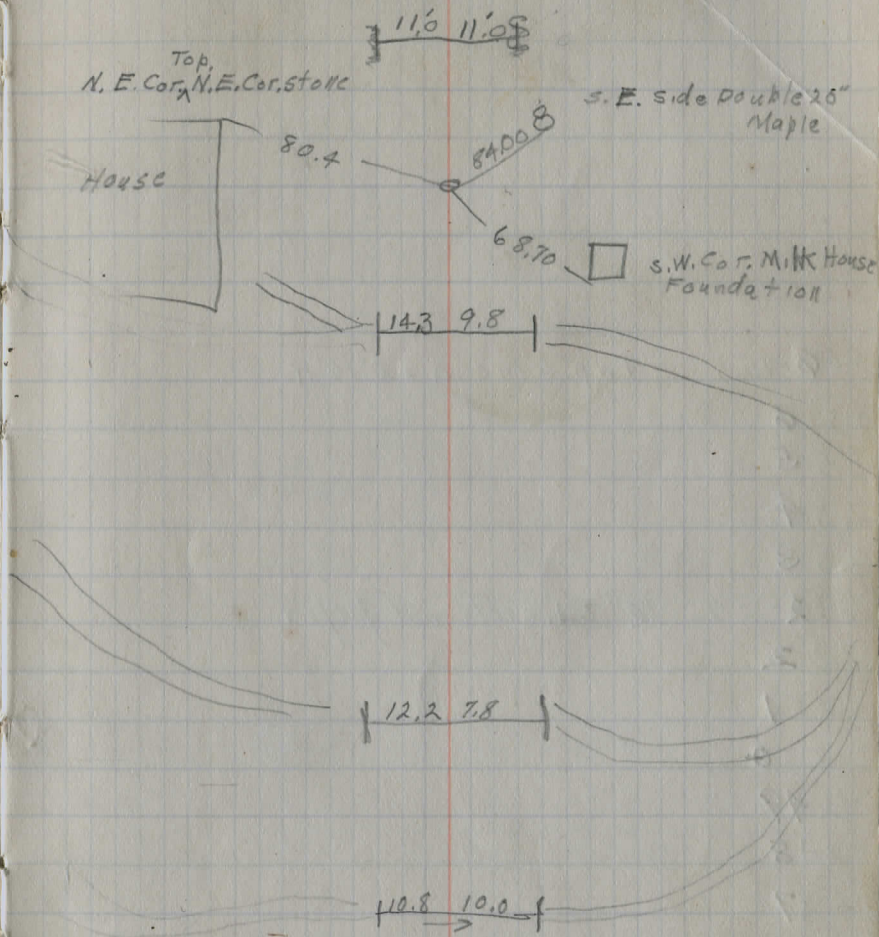
Oct. 27, 1923
Fair

Marks
Gray
Thompson

37



- 239+25 4" Drain Tile No. H. W. S.
 239
 238
 237+593 Iron Pin $\Delta = 0^{\circ}00'$
 237
~~236~~
~~235~~
 234+91 10" c.i. 1/2 sectional Pipe
 234
 233
 232
 231
 230
 229
 228+40 Stone Box 3' x 2'
 228
 227
 226
 225+27 Plank Box 18" x 12" ^{30 acres ±} Dramage Area
 225
 224
 223+130 Cross Roads Co. Hwy 13
 223 Chardm - Windsor
 222 SAN
 221
 220



256+15.5 Twp. Line A = 0°16' R.

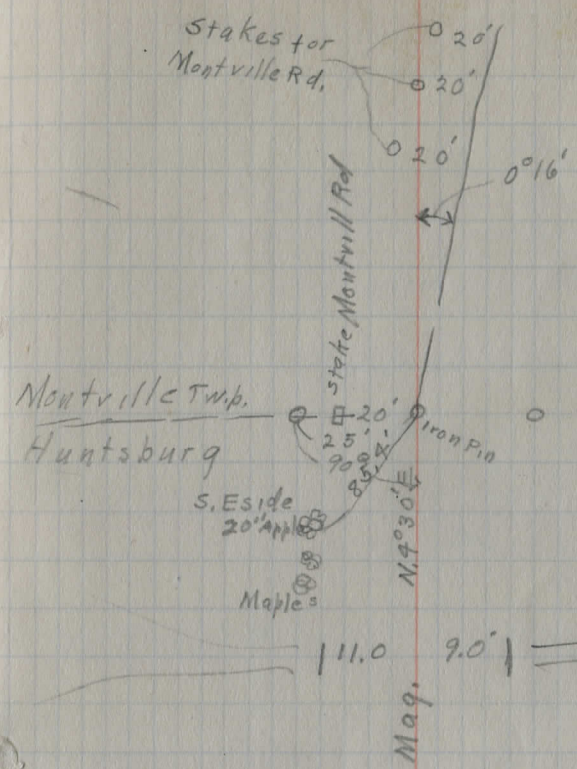
- 256
- 255
- 254
- 253

252+22 12" cil. sectional p/p's

- 252
- 251
- 250
- 249
- 248
- 247
- 246
- 245

244+31.5 stone Box 62" x 32" x 16.0
 Poor. W. End Fair, E. Half,

- 244
- 243
- 242
- 241
- 240

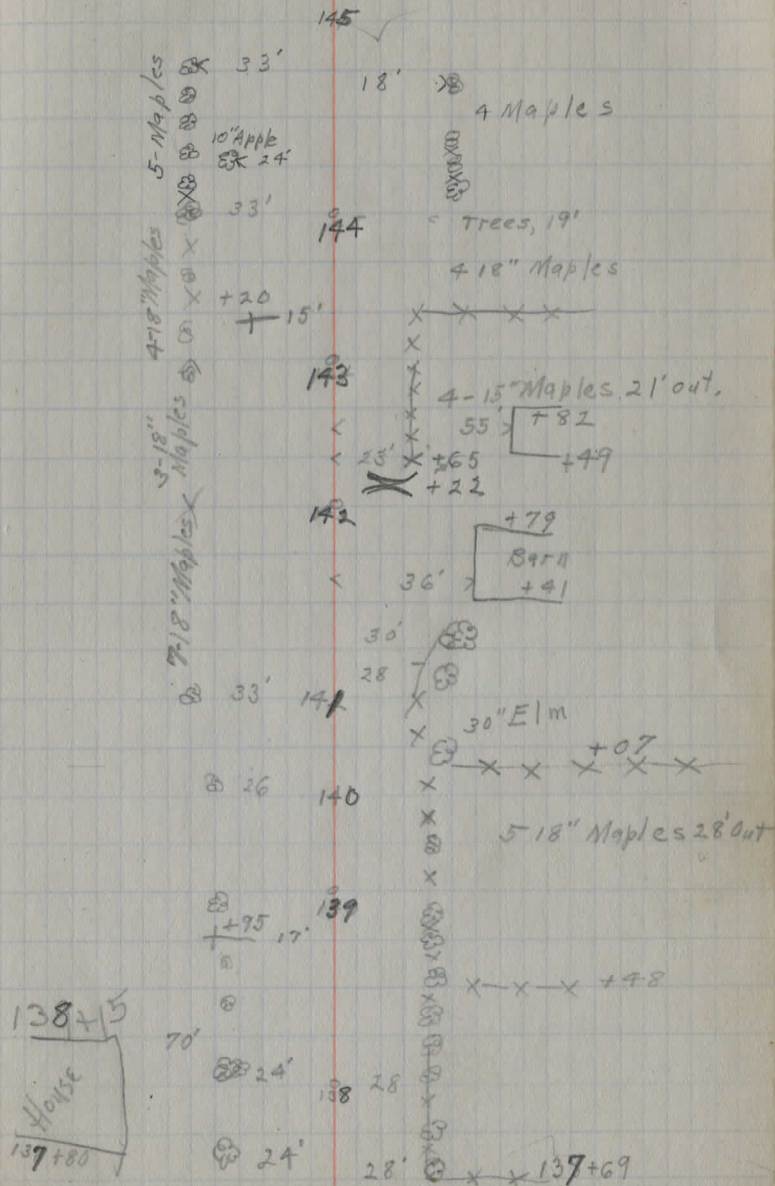


25' 0

Fore-noon Oct. 29, 1923
Fair

Marks
Gray

40



155

X

+75 + 18'

134

27' Locust X 34'

X
153

+50 + 17'

20' X +60
18" Hickories
25' X +50

+80 18" Maple X 33'

152

26' X 15" Maple X
20" Locust
23' X X X X +58

+22 X X X

22' X 18" Locust

Locusts

151

22' X 24" Locust

+17 + 18'

18' X 2 Maples 18"

150

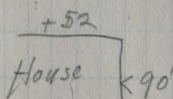
30" Maple X 30'

19' X 30" Hickory X 22'
+92
12" Apple X 24

18" Walnut X 30'

31' 149 18.5

5 Maples 18"



3-15" Maple

+43 X X X

+80 31' X
+95 20' X

4 15" Maples
X X X +43

4 Maples X 33' 147

3-18" Maples

4 Maples X 146

+67 19 7

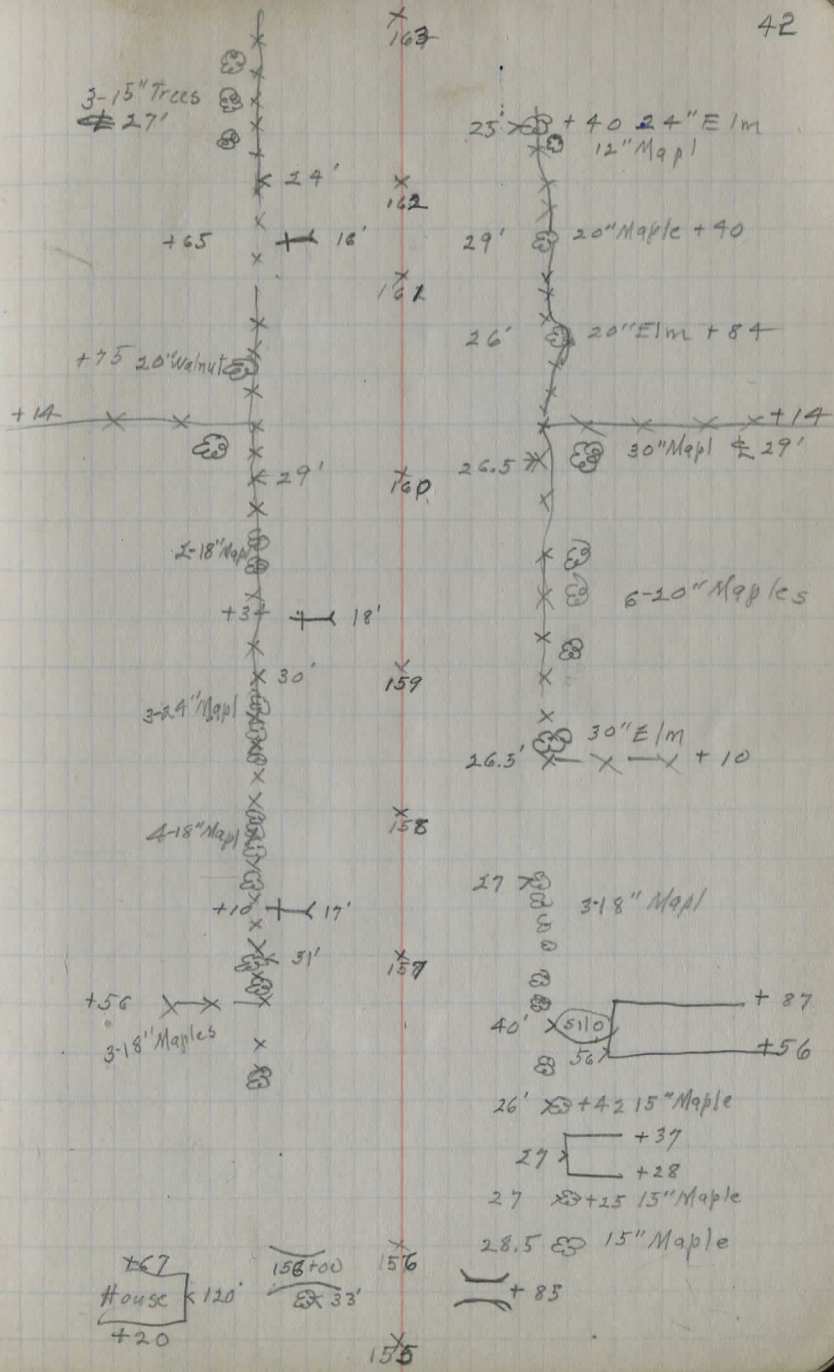
18" X Maples

1-18" Maple

18' X 4-18" Trees

33 145

19' X Apple



3-15" Trees
~~27'~~

24'
162
29'

+75 20" Walnut

+14

2-18" Mapl

+3 18'

3-24" Mapl

4-18" Mapl

+10 17'

+56
3-18" Maples

267
House 120'
+20

156+00
33'

163

25' +40 24" Elm
12" Mapl

29' 20" Maple +40

26' 20" Elm +84

+14
26.5' 30" Mapl 29'

6-20" Maples

26.5' 30" Elm +10

17' 3-18" Mapl

+87
40' 510
56' +56

26' +42 15" Maple

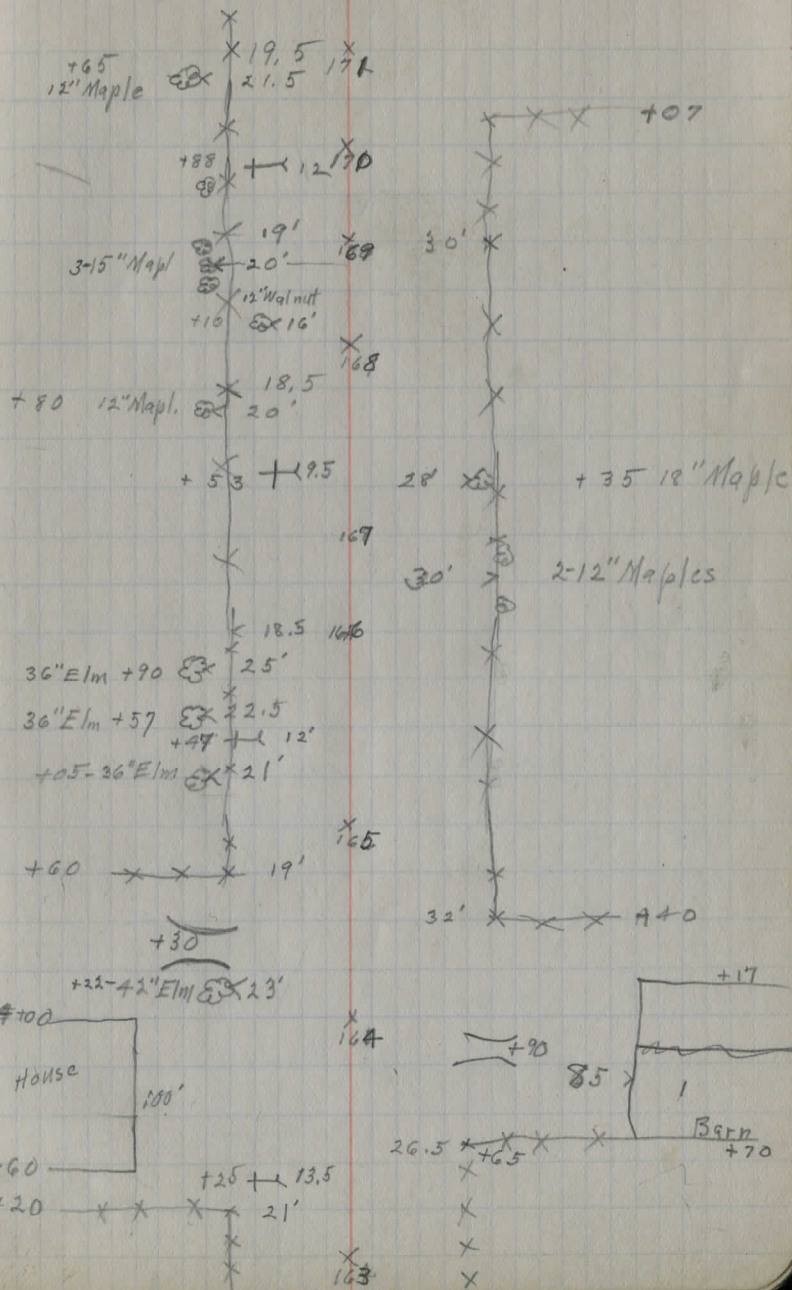
+37
27' +28

27' +25 15" Maple

28.5' 15" Maple

+85

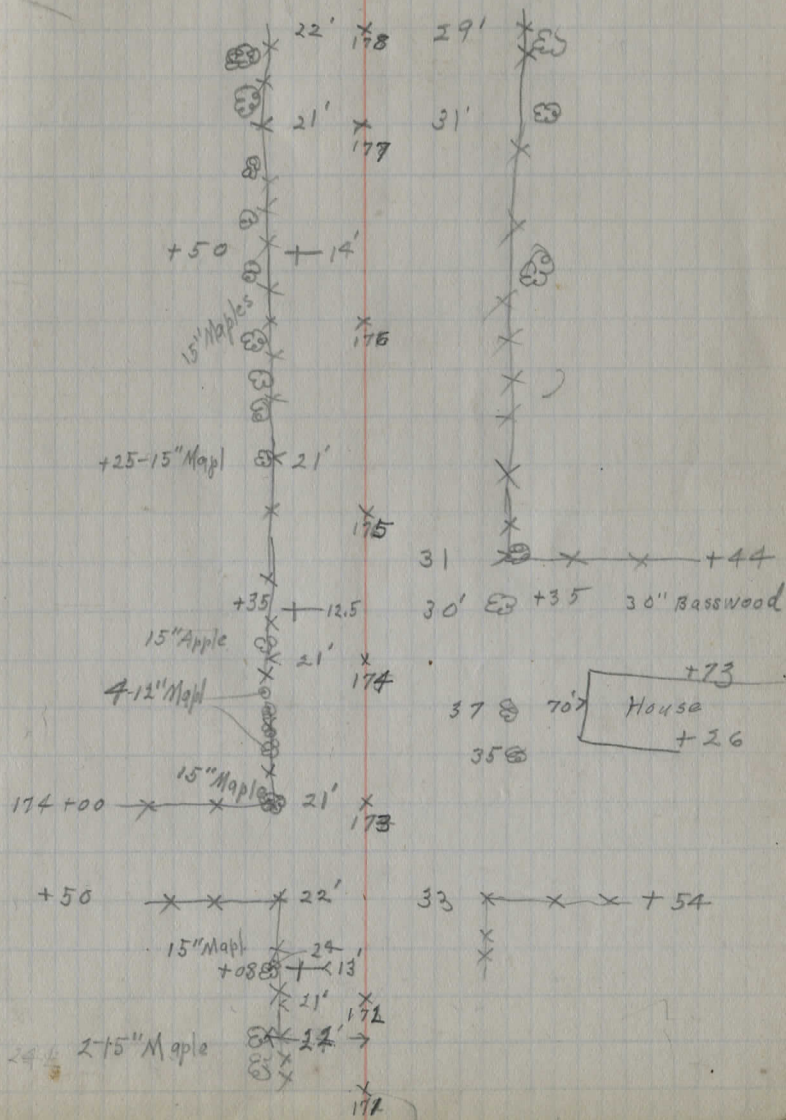
155



Oct. 30, 1923
Rainy

Marks
Grau
Thompson

44



25 ^x206

30 ⊙

28 ⊙

^x205

180 + 12

30 ⊙

15

22 ^x204

14

30 ⊙

28 ⊙

15 + 12.5 ^x203

28 ⊙

23.5 ^x202

^x201

150 + 14

21 ^x200

+63

24 199
23.5

30

+65

Brush

129 + 14

198

31

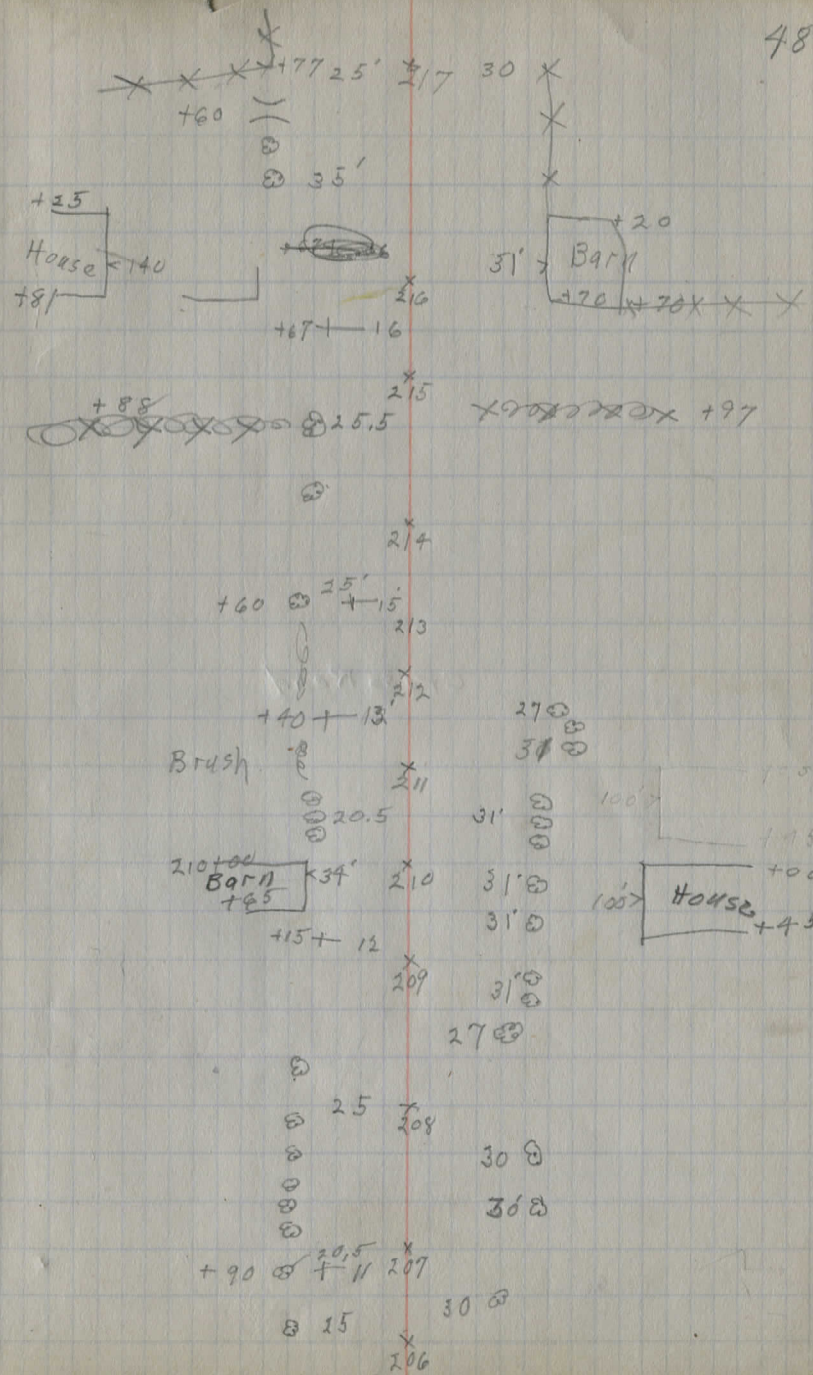
197

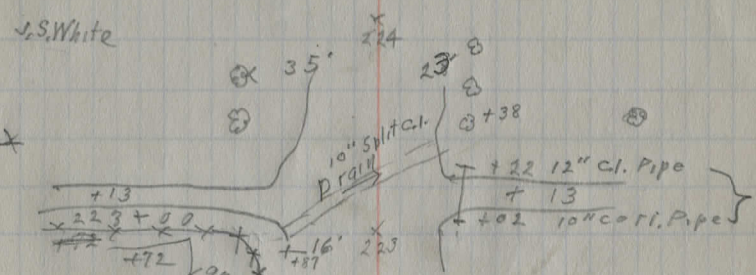
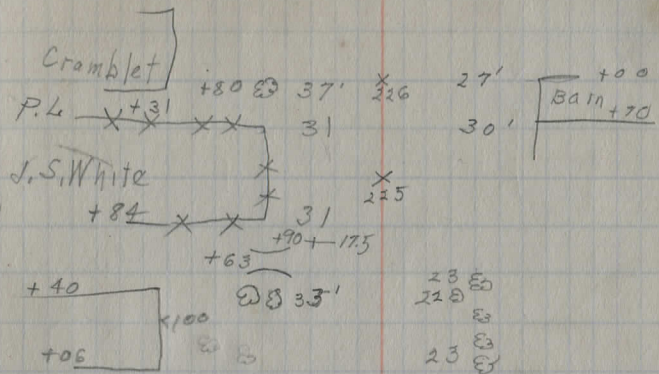
26.5

+10 + 14

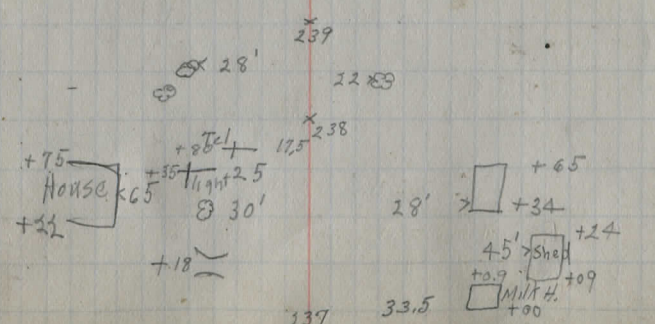
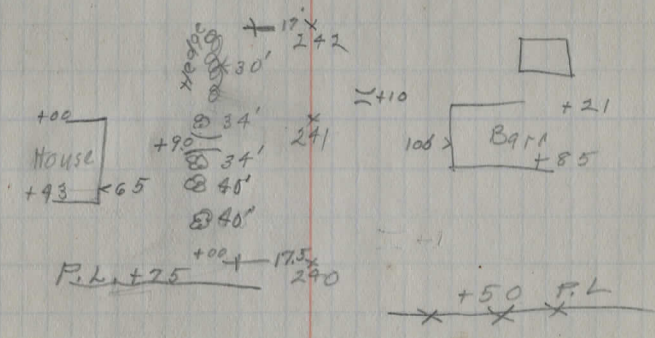
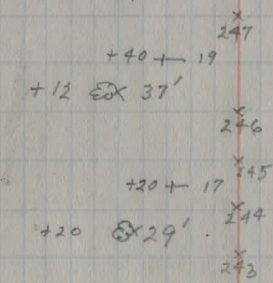
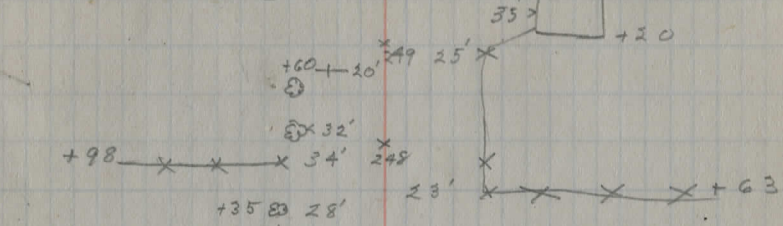
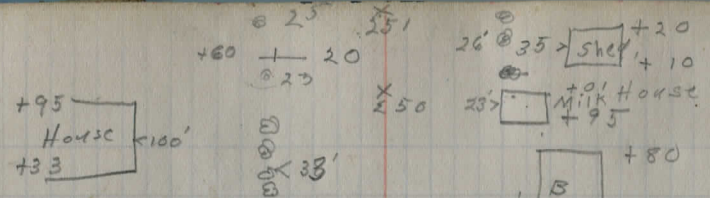
25 ⊙

^x196





Cross Road



Fl. +15.5
Twp Line X X X X X 32.5

26' ~~X X X X X~~ +10

X
256

CB

255+00
House } 85 185 34' 255
+58 } +58

+40 20

X
254

+35 31

25 30 +30

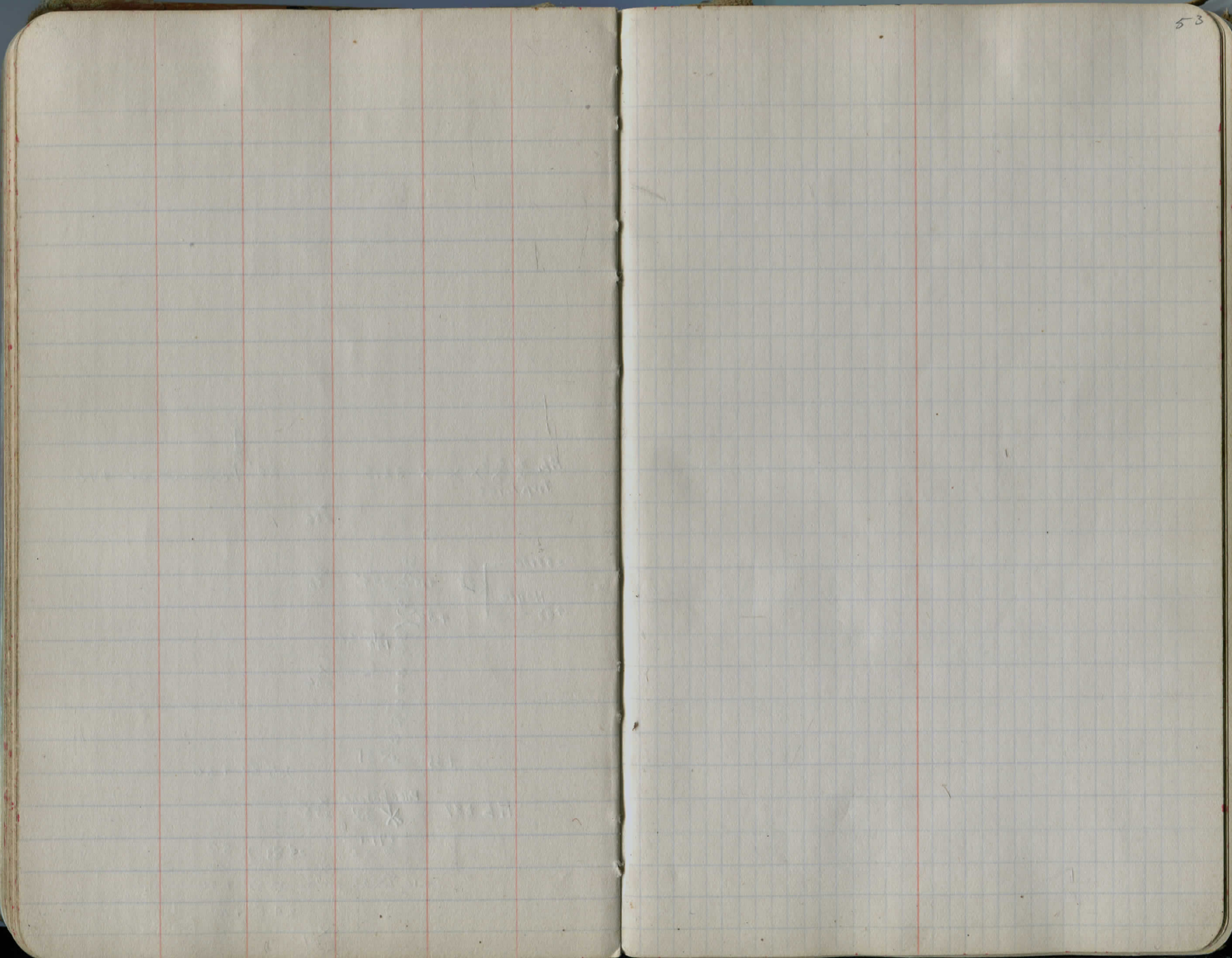
Fl. +87 Pilcot Stone X
X 33' 258

+79 +20
25 23 30 +50

+10 25 252 23 30 +50

24 30 +10

X
251



Alignment Survey of N. + S. Road,
1 mile W. of Huntsburg Center, N. from I.C.H. 15
5 stakes set on offset 25' R. of \pm unless
otherwise noted "Gloy Street" C.H. # 37

39+00 $\Delta = 0^{\circ} 31' R.$

Note: —

See next set of notes for
restaking. Sta 0+00 on re-
staking = Sta 134+15 of old notes
Sta. 134+13.42 on restaking
= Sta. 0+00 of old notes

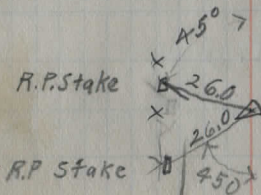
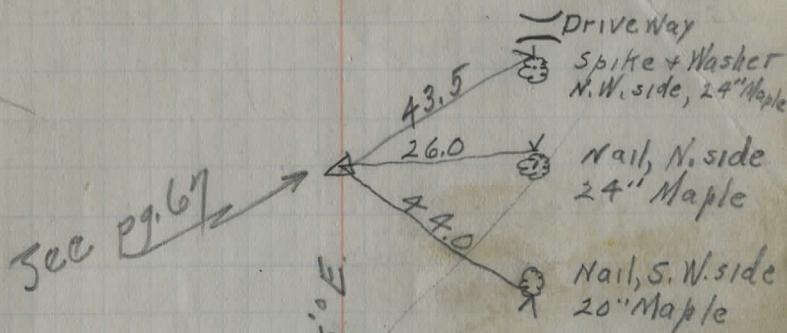
20+00 $0^{\circ} 00'$

0+00 2" Drill Hole, 1' N. of S. edge of concrete

June 22, 1926
Fair.

Marks
Grav
Parks
Canfield

55



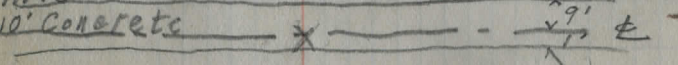
see pg 69
Hub

see pg. 71

I.C.H. 15

10' Concrete

AA # 322



95+00

0°00'

86+00

$\Delta = 0°00'$

70+00

$\Delta = 0°20'R.$

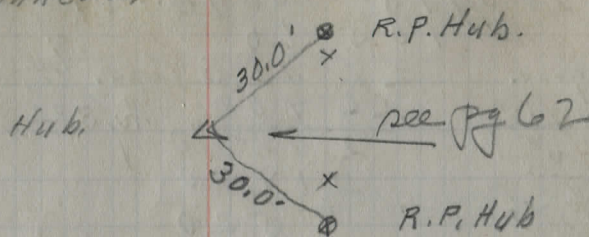
Sta 50+31

1. PIPE FD RAISED MAY '54

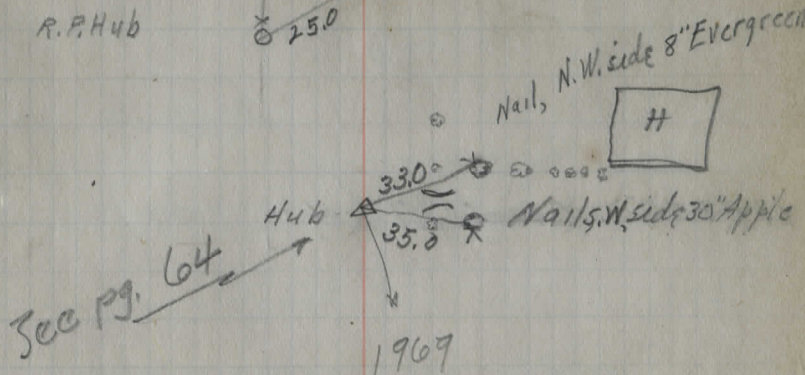
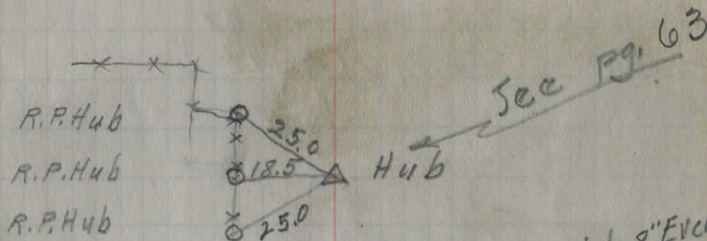
APPROX

113'
31'00"

stopped June 22,



25' x



CENTER STEEL SIGN POST SET IN CONCRETE

E. E+W. Rd.

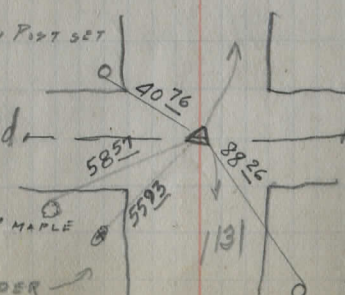
Huntley Rd

NOT B.M.

VERT SIGN N. FOOT 24' MAPLE

CRISTOP BOULDER

SEW NE. SIDE CEI * 555199



134 + 15
9

miles

5-250 / 134 + 06 / 2.57 - 5.2

105	60	
28	460	Gas. \$4.815-50
26	400	Av. 300, 1/2 mi
<hr/>		
20600		
21120		
<hr/>		
5.20		

15 grass.
25 loading
45 haul
5 sign
0 1/2 fuel
10

4965 Ch. yds 12" x 10' x 134 + 06
35 " " " " " "
5000 " " " " " "

134 + 15.0 Township Line

114 + 00 Δ = 0°27' Left

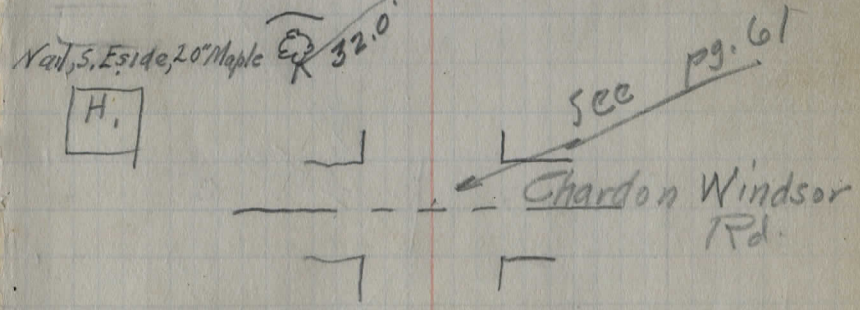
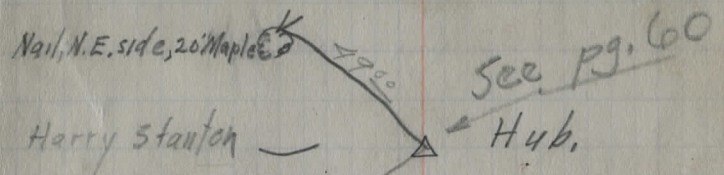
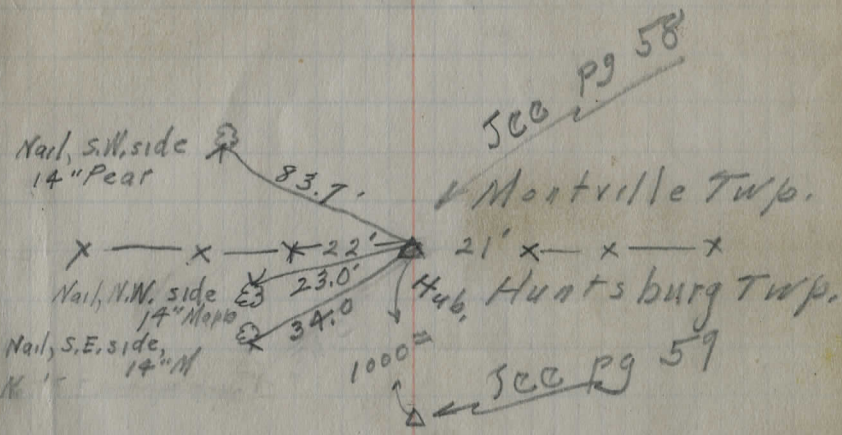
100 + 87 ^{cl} E + W. Road

Iron set
6/1/33 1199

95 + 00

June 22, 1926, P.M.
Windy, after Rain

Marks
Grau
Parks
Canfield 57

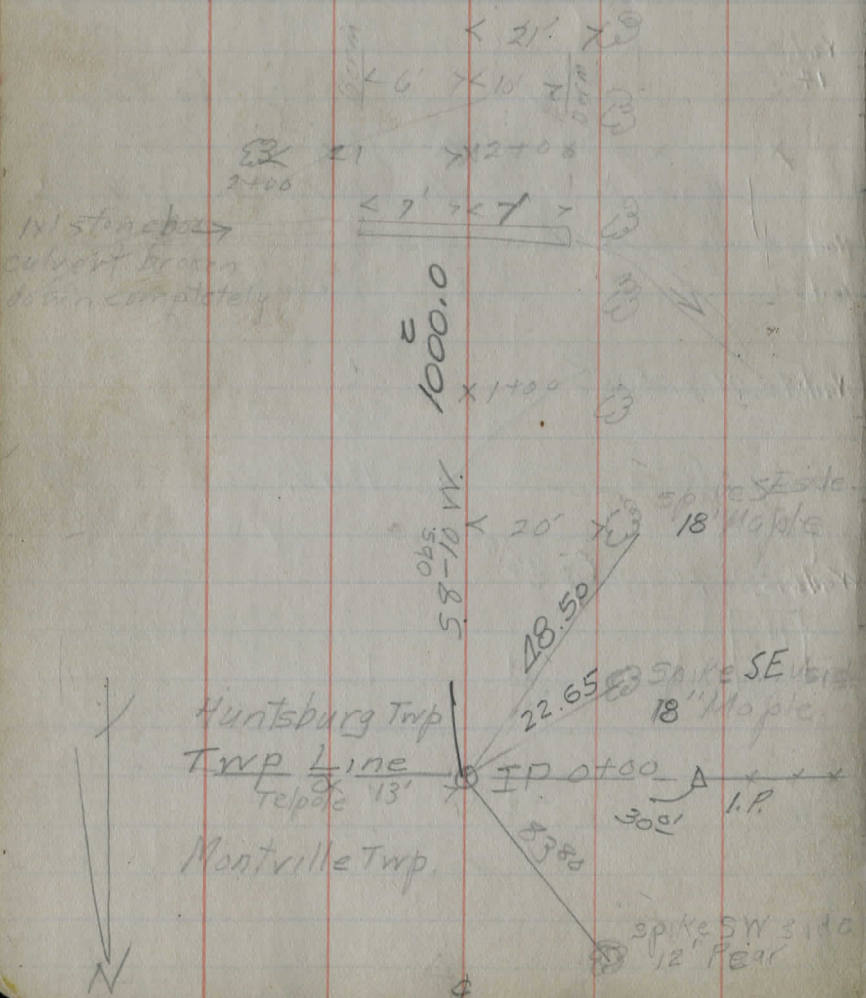


△

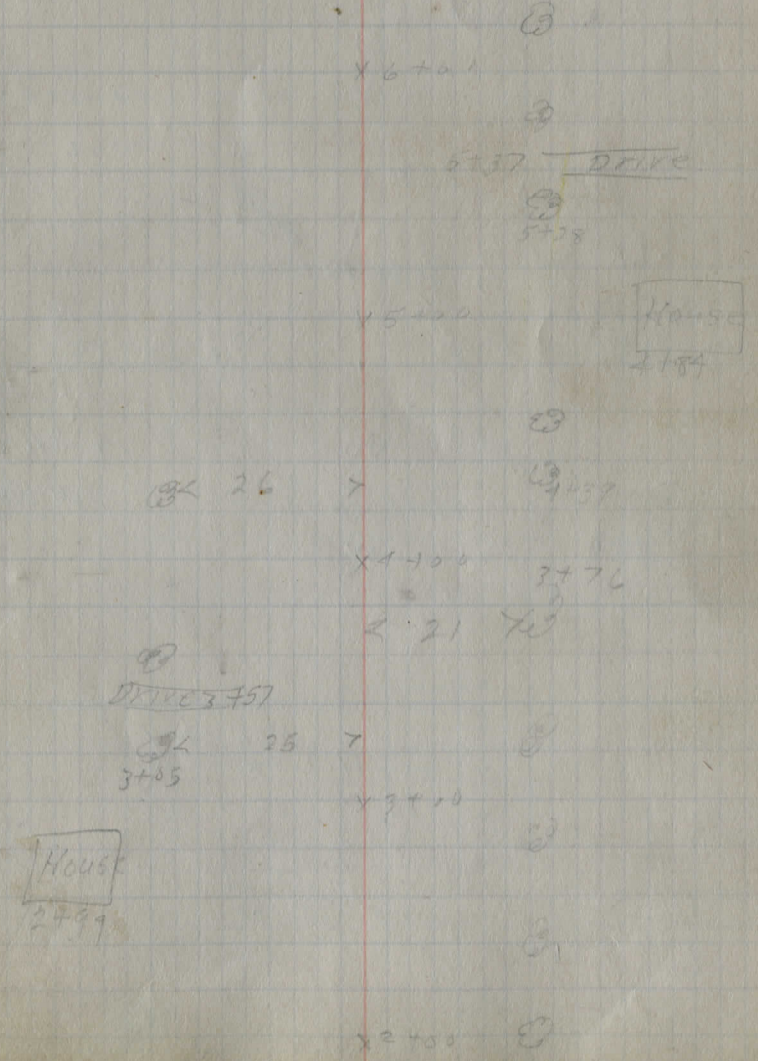
Restaking of Clay Street from
Huntsburg-Mantville Twp. Line South

7/12/27 Richey
Randal
Canfield

side stakes are 25' E or Left Goodrich

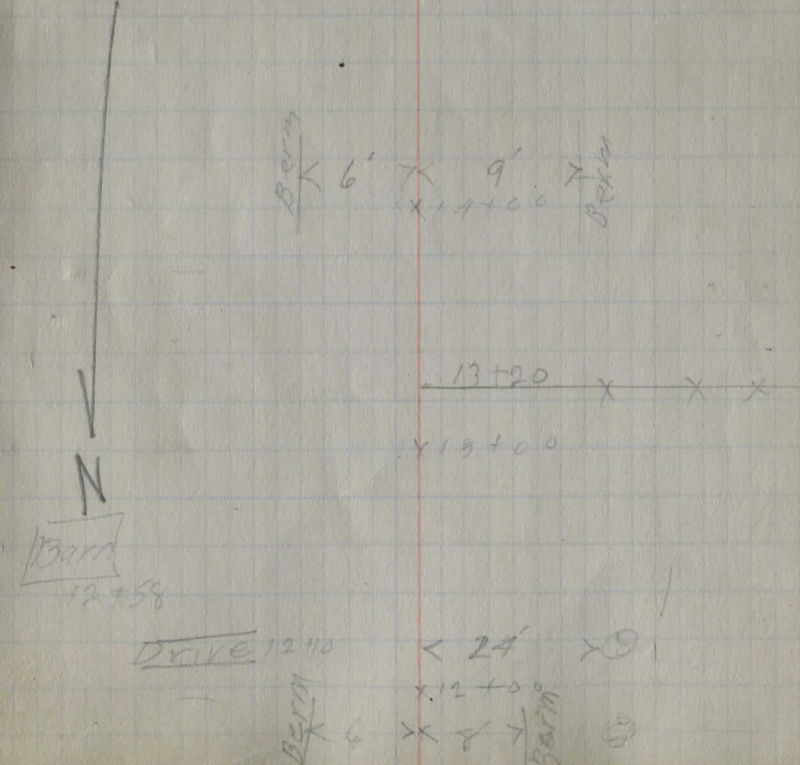
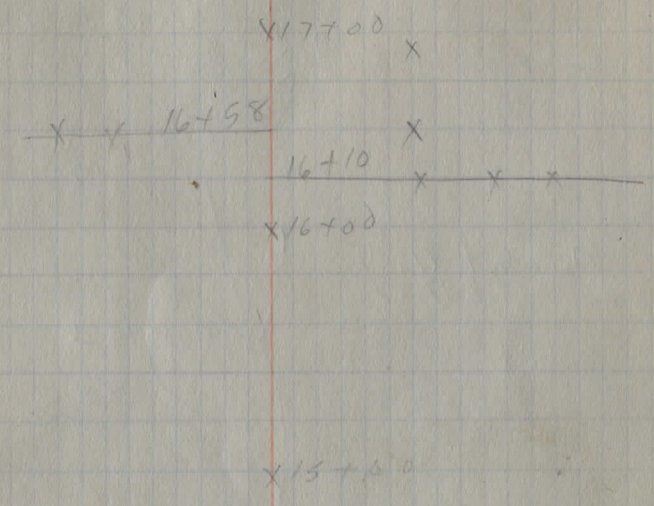
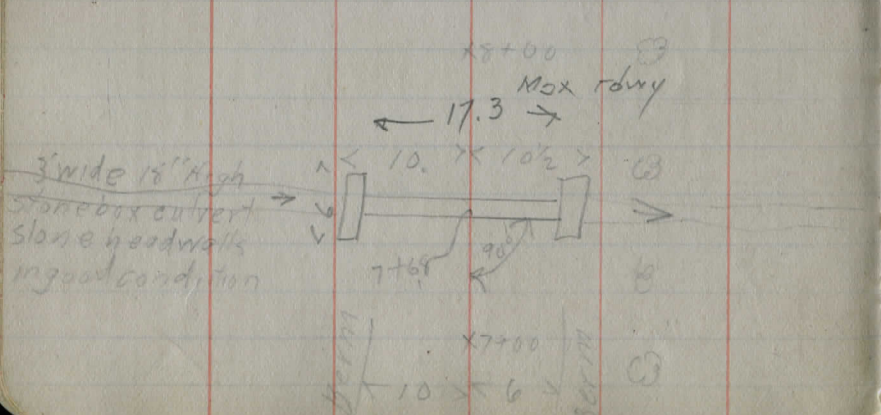
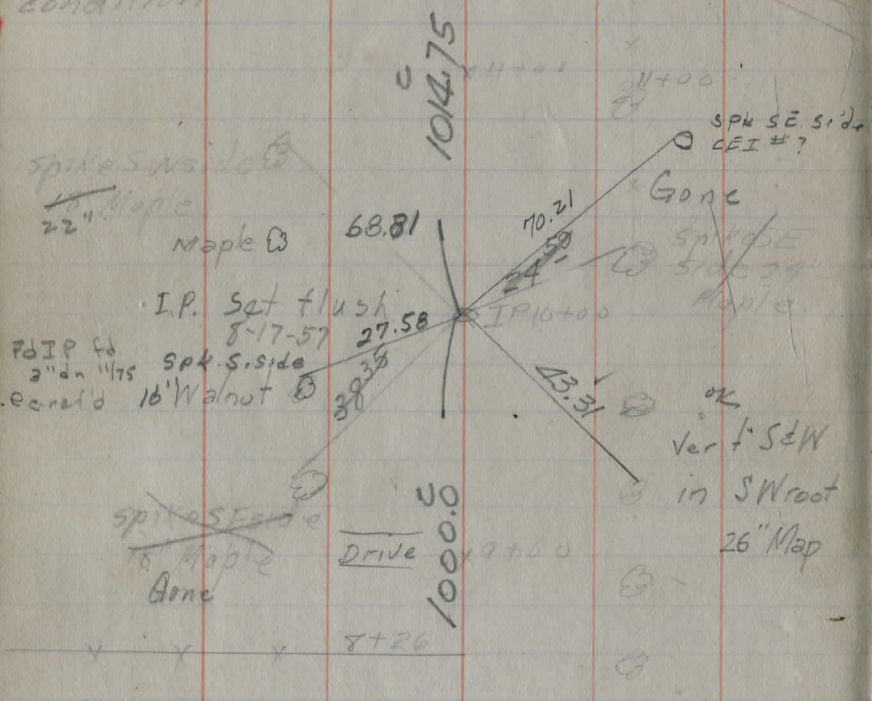


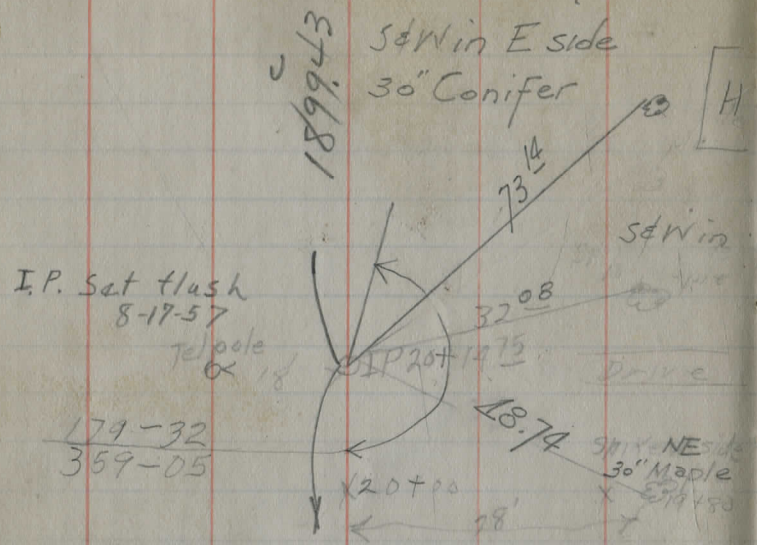
NOTE: All points $\times 7+100$
except 33+27 $\angle 29$ $\times B$
Found & referenced
Apr. 1952



House
11714

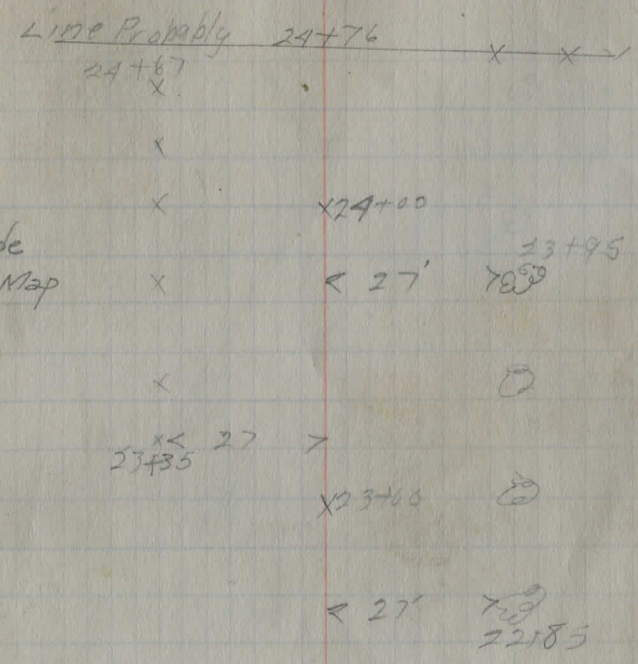
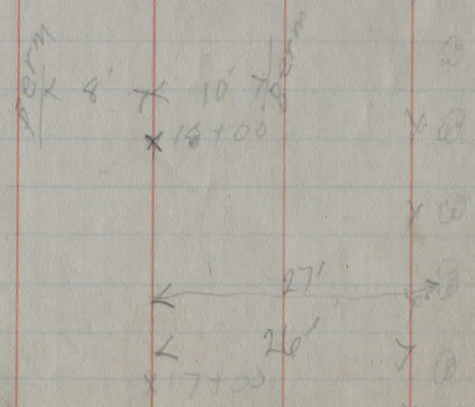
12" Corrugated
IP in good
condition





179-32
359-05

1012.75
X 19+00



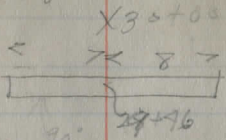
House
21+31

DRIVE 20+72

IP 20+14.75

Te/p.
OK 18'

10" corrugated
IP in good
condition



X 29+00

DRIVE 28-85

House
25+35

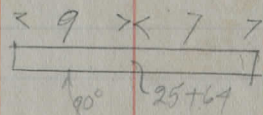
OK 29
27+97

X 28+00

Berm
X 8' X 7' X Berm
X 27+00

X 26+00

12" corrugated
IP in good
condition

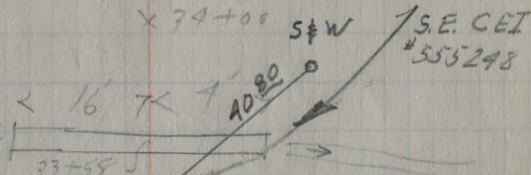


X 25+00

SEE FB313 FOR
1975-76 DATA AND
THIS AREA

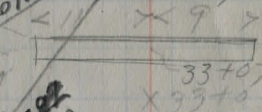
No Find 4-52

12" CIP in
good condition



Road
I.P. Set flush
8-17-57

12" CIP in
good condition



S&W
12" Elm
S&W
Twin 8" Elms

CHARDON-
WINDSOR
CH #13

DRIVE 31-97

House
31+97

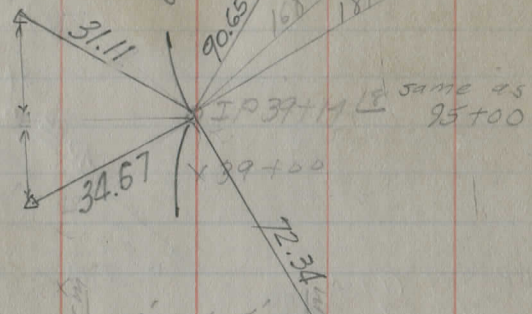
1899.43

X 32+00

X 31+00

X 30+00

S&W in NW side CEI
NEA Foundation on 90773 NW Foundation



SEW in NE side CEI # 555245
6' x 5'
x 22 x 38+00
37+58

DRIVE 37+25

37+05
1899.43
x 37+00

29
x 36+00

DRIVE 36+03

WR 40'
x 35+00

House

35+47

6' x 6'
21' x 35+00
Tep

School House

House
44+58

DRIVE 45+38

44+38
35'

orchard

FLIMS Barn 38'
43+45

42+40

41+55

Fence & Tep Pole
23' x 41+00

x 46+02
45+65

x 45+0 x
44+76 x x x

x 44+0

x 43+00

x 42+00

Probable school house S. Line

Barn
49+85

30' x 50+10
DRIVE 49+98

1600.08

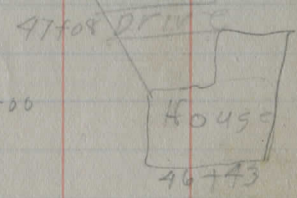
Spk NW side
CEI #
555238

48+13²² IP
I.P. Sat flush
8-17-57

25° I.P. rocks

Gone '75
I.P. fence
brace
(ctr 6" above
ground)

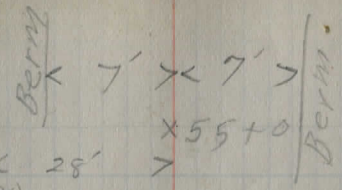
899.32



House
46+43

23' x
46+00

54+90

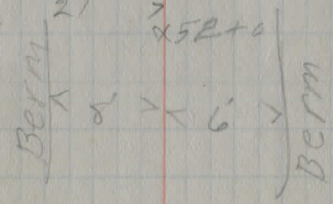


54+8

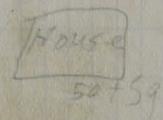
53+0

DRIVE 52+54

Telfox 21' x 52+0



51+00

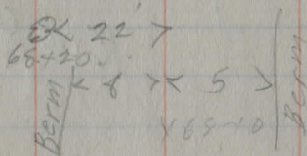


50+59

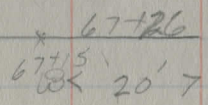
50+10

X70+0

X69+0



X 21' \rightarrow 67+69



X67+0

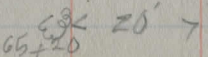
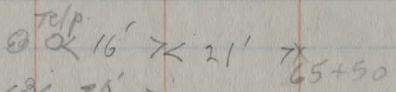
⊙

⊙

⊙

⊙

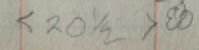
X66+00



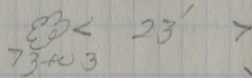
DRIVE 65+10

X65+00

64+95



X76+0

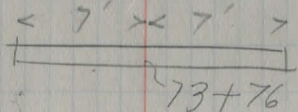


X75+0

FCP
 3099.98

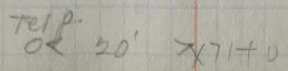
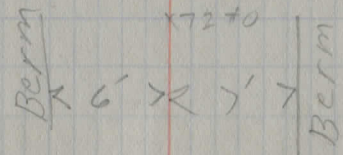
X74+0

1x1' wood
 box culvert
 in fair
 condition



X73+0

X72+0



0 0 0
0 0 0 80793 X8110

DRIVE 90777

House
80710

0 0 0 80710
0 0 0 X8070

0 0 0
vineyard

0 0 0
0 0 0 X187
79728

X7970

N

Telp. OK 13' 7" X7810

< 36 70 70 70

77768 Drive

X 77744

X7770

House

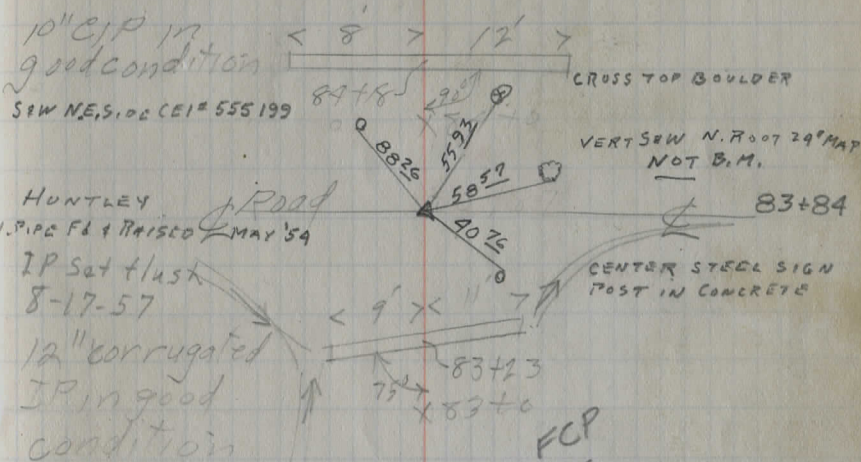
77756

Berm X5 X6' 7" X7670
Berm

66

Berm X
3' 7" X8670
Berm

Telp. OK 14' 7" X8570



FCP
3099.98

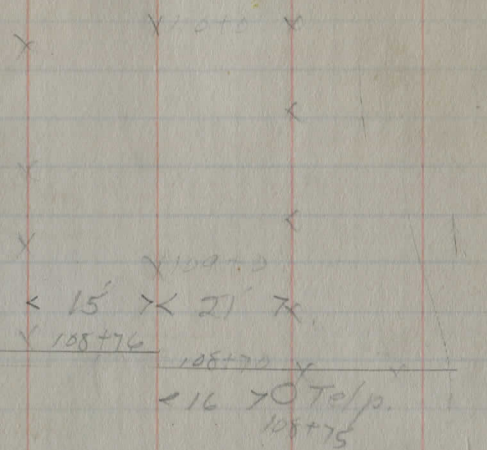
X8270

81+97

0 0 0

0 0 0 < 19' 7"

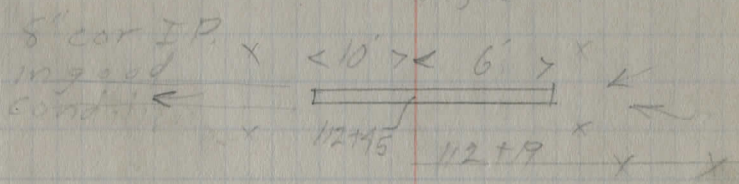
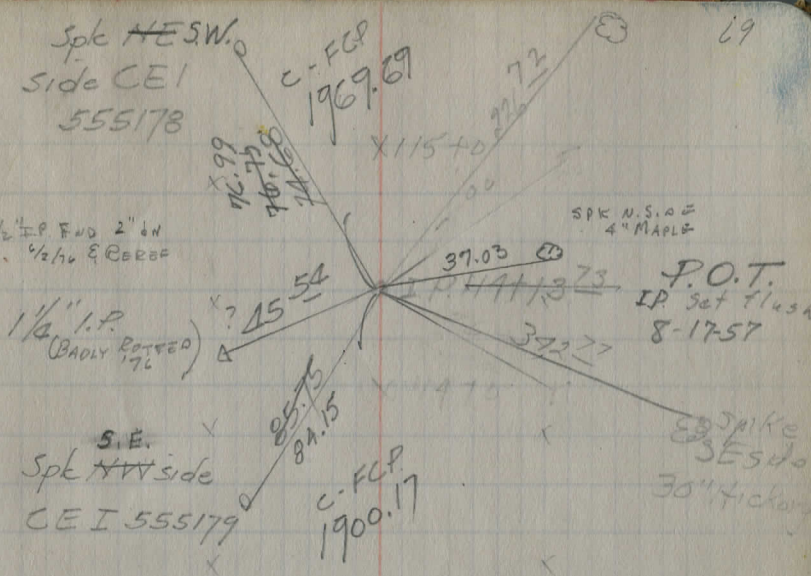
0 0 0 X8170



1999.69
 1900.17
 3899.86

N

X 108+0
 X 107+0
 X 106+0
 X 105+0
 X 104+0

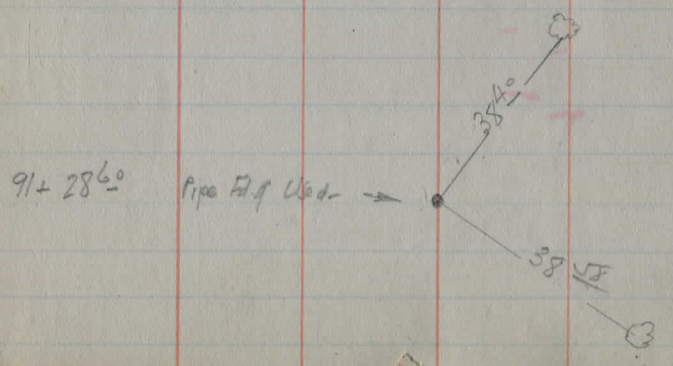
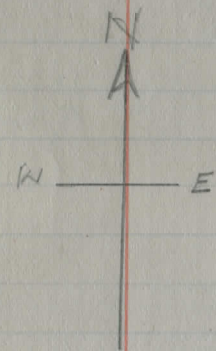
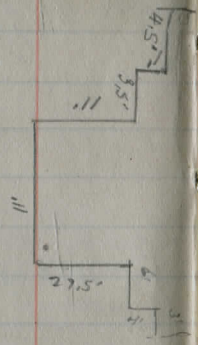
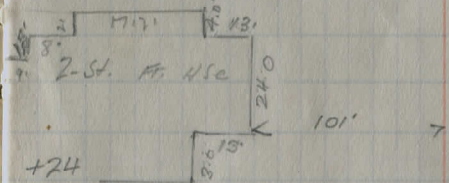


X 113+0
 X 112+0
 X 111+0
 X 110+0

MADISON ROAD SR #528
 South of #322
 (Probably)

Feb. 28, 1933 (Fair) Temp. 32°
 M. B. Richey - Tr.
 R. Goodrich - Chairman
 S. Gold Jr. - Rec.

- +52 3" Pine @ 27.5'
- +47 6" Pine @ 28'
- +40 29' @ 12" Orange
- +39 6" Pine @ 27.5'
- +24 2-St. Fr. Hse 101' 7
- +19 8" Pine @ 28'
- +16 4" Pine @ 28'
- +14 C.C. @ 23.5'
- +12 4" Pine @ 27.5'
- +08 6" Pine @ 27'
- +7+0 3 @ 30.5' < 28.5'
- +78 Low @ Pines 15" 28' @ 0 1/2 Orange
- +91 Drive (No Pipe Placed)
- +74 18.7 @ T.P.
- +53 28.5 24" Orange
- 91+28.60 29.5'



+65

+78

+26

+05

9410

+70.5 (to Culvert)

+62

+55 CEI. hole @ 23'

+51

+00 wire fence

93 to 17" pipe @ 27'

old chicken
coop
+975 10' x 11'

+85

+79 + Dr. Corr. Pipe

+57

+65

92-156 6" Pipe @ 28'

Spring
210
5'

152'

28'

28'

16.5'

15.5'

31'

18' @ T.P.

191'

52.5'

28'

End of wire
Bag of Rail & Nails
1.3' high

15' 2' 2 1/2'

24' @

12" Locust Stub

14" x 2" wire fence

Wire fence

12" o'sage

5'

C

14" Pines

14" Pines

(100+18[?]) \neq Drive \downarrow

+18

+15 C.E. 1.16/2 \odot 22'

99+12

+96

+89 6" Maple \odot 29'

+87

+67 12" Maple \odot 31'

98+55

2nd Fr
N5C

\neq Drive \downarrow

235' \odot C.E. 1.16/6

\neq Drive \downarrow

Sta	+ H.I.	-	Elev.	Rem's
B.M.	7.14	1180.86	1173.77	
(88+0)				
91+28.60			1177.9	
92+0			1178.0	
92+50	(G.L. Witness Stood Elev. 1183.70)		1177.3	
93+0			1176.8	
T.P.	9.57	1186.20	4.73	1176.63
93+50			1176.5	
94+0			1176.8	
+76.	(T/Stone Elev. 1177.20)			
94+50			1178.0	
95+00			1179.8	
+50			1181.9	
96+0			1185.0	
T.P.	12.02	1198.04	0.18	1186.02
96+50			1188.2	
96+09	Elev. by Apple Tree 1190.2			

West	±	East
	10.7	
	3.0	
	2.9	
	3.6	
	4.1	
	9.7	
	9.4	
	8.2	
	6.4	
	4.3	
	1.2	
	9.8	

Sta	+	K.I.	-	Elev	Paralle
97+0		1198.04		1191.5	
97+50				1194.8	
+76		T.R. (CE 1.86 5.0)			
98+0				1197.9	
T.P.	11.38	1209.27	0.15	1197.89	
98+50				1201.0	
98+40		(Highest Point on Line of Sight 1207.7)			
99+0				1204.0	
99+50				1206.8	
T.P.	10.00	1218.71	0.56	1208.71	
100+0				1209.7	
+18				1210.7	
101+0				1215.6	
T.P.	12.54	1230.66	0.59	1218.12	
T.P.	12.17	1242.49	0.32	1230.32	
T.P.	12.35	1254.84	0.00	1242.49	
T.P.	6.34	1259.88	1.30	1253.54	
B.M.			3.38	1256.50	B.M See plans -

West	E	East
	6.5	
	3.2	
	2.5	
	8.3	
	5.3	
	2.5	
	9.0	
	8.0	
	3.1	

	+	N 1	-	
B.M.	3.38	1261.35		1257.97
T.P.	0.28	1250.41	11.22	1250.13
T.P.	1.11	1240.15	11.37	1239.04
T.P.	0.82	1229.03	11.94	1228.21
T.P.	0.48	1216.52	12.99	1216.04
T.P. B.M.			6.36	1210.16
T.P.	0.74	1206.46	10.80	1205.72
T.P.	0.07	1194.42	12.07	1194.39
T.P.	0.26	1182.64	12.08	1182.38
B.M.			6.16	1176.48
T.P.	1.72	1180.69	3.67	1178.97
B.M.			6.96	1173.73

S.W. Corner
of window
at school
Sta 93+70

W E
4+0 8' 11'

Stks set 12' E
6+0 10' 14'
8+0 9.5' 14'
10+0 stks 8.5' 14.5'
12+0 " " 8.5' 16'
14+20 to 15+70 10" VSP on W
16 9' 14'
18 9' 13'
19+99.6 P.O.T
20 9.5' 14'

W E

26+0	11'	12'
28	12'	12'
30	12'	9.5'
32	12	9'
34	11	8.5
36	9	9
38	9	9
38+99.33	PI	
40	11	8.5
42	11	8.5
44	11.5	9
46	13	8
48	11.5	9.5
50	12	9.5
52	13	8
54	12	8.5
56	11	8.5
56+88 to 58+41	NEEDS delc4 now (SPTENT)	
58	11.	8
60	10.5	9.5
62	10	10.5
64	9.	11
66	8.5	11.5

57.97
56.50
1.29

8069 10.56
147 1.57
79.32 07.09
73.22
75.0

78
76.52
705 1.57
1307

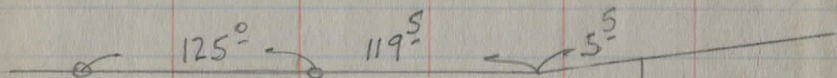
7100 WOODS ST

6.50

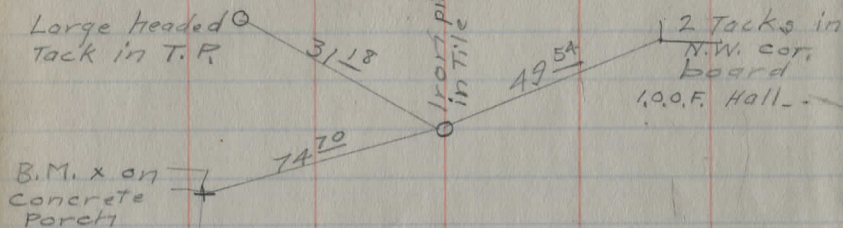
119.5
125

244.5

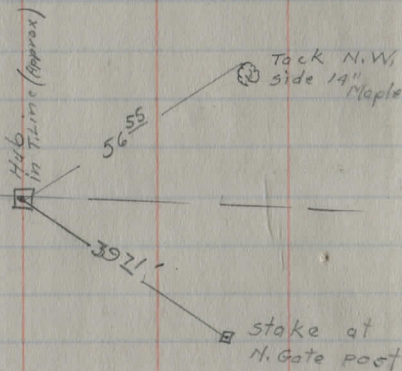
100.00



Ref. at Huntsburg Ctr.



Ref. at Town Line



DIRECTIONS FOR USE OF TABLES

TABLE No. 1

52.13
1227.85
422

Distance to slope stake from side or shoulder stake for any width roadway, slope 1% to 1%. If ground is nearly level, the cut or fill at side stake is located by the 50 ft. curve method in left column and top row. The number in body

IMPROVED TABLES

AND

INFORMATION

TABLE No. 2

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of correction. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius of the curve.

39+14 L8
25
159

DIRECTIONS FOR USE OF TABLES

288
15650
13.50

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

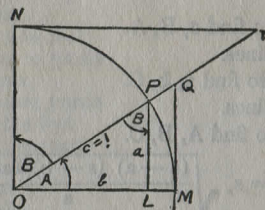


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30°
1°	50.00	.218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10°	58.34	.297	5° C.	10°	560.11	27.313	5° C.	10°	1070.6	99.155	5° C.
20°	66.67	.358	T	20°	568.53	28.137	T	20°	1079.2	100.775	T
30°	75.01	.491	E	30°	576.95	28.974	E	30°	1087.8	102.35	E
40°	83.34	.606	.03	40°	585.36	29.824	.06	40°	1096.4	103.97	.10
50°	91.68	.733	E	50°	593.79	30.686	E	50°	1105.1	105.60	E
2°	100.01	.873	.001	12°	602.21	31.561	.006	22°	1113.7	107.24	.013
10°	108.35	1.024	10° C.	10°	610.64	32.447	10° C.	10°	1122.4	108.90	10° C.
20°	116.68	1.188	T	20°	619.07	33.347	T	20°	1131.0	110.57	T
30°	125.02	1.364	E	30°	627.50	34.259	E	30°	1139.7	112.25	E
40°	133.36	1.552	.03	40°	635.93	35.183	.06	40°	1148.4	113.95	.10
50°	141.70	1.752	E	50°	644.37	36.120	E	50°	1157.0	115.66	E
3°	150.04	1.964	.003	13°	652.81	37.070	.011	23°	1165.7	117.38	.025
10°	158.38	2.188	10° C.	10°	661.25	38.031	10° C.	10°	1174.4	119.12	10° C.
20°	166.72	2.425	T	20°	669.70	39.006	T	20°	1183.1	120.87	T
30°	175.06	2.674	E	30°	678.15	39.993	E	30°	1191.8	122.63	E
40°	183.40	2.934	.06	40°	686.60	40.992	.13	40°	1200.5	124.41	.19
50°	191.74	3.207	E	50°	695.06	42.004	.011	50°	1209.2	126.20	.025
4°	200.08	3.492	.003	14°	703.51	43.029	.011	24°	1217.9	128.00	.025
10°	208.43	3.790	15° C.	10°	711.97	44.066	15° C.	10°	1226.6	129.82	15° C.
20°	216.77	4.099	T	20°	720.44	45.116	T	20°	1235.3	131.65	T
30°	225.12	4.421	E	30°	728.90	46.178	E	30°	1244.0	133.50	E
40°	233.47	4.755	.03	40°	737.37	47.253	.06	40°	1252.8	135.35	.10
50°	241.81	5.100	E	50°	745.85	48.341	E	50°	1261.5	137.23	E
5°	250.16	5.459	.004	15°	754.32	49.441	.017	25°	1270.2	139.11	.038
10°	258.51	5.829	15° C.	10°	762.80	50.554	15° C.	10°	1279.0	141.01	.070
20°	266.86	6.211	T	20°	771.29	51.679	T	20°	1287.7	142.93	T
30°	275.21	6.606	E	30°	779.77	52.818	E	30°	1296.5	144.85	E
40°	283.57	7.013	.06	40°	788.26	53.969	.13	40°	1305.3	146.79	.19
50°	291.92	7.432	E	50°	796.75	55.132	E	50°	1314.0	148.75	E
6°	300.28	7.863	.006	16°	805.25	56.309	.022	26°	1322.8	150.71	.051
10°	308.64	8.307	15° C.	10°	813.75	57.498	15° C.	10°	1331.6	152.69	.083
20°	316.99	8.762	T	20°	822.25	58.699	T	20°	1340.4	154.69	T
30°	325.35	9.230	E	30°	830.76	59.914	E	30°	1349.2	156.70	E
40°	333.71	9.710	.03	40°	839.27	61.141	.06	40°	1358.0	158.72	.10
50°	342.08	10.202	E	50°	847.78	62.381	E	50°	1366.8	160.76	E
7°	350.44	10.707	.006	17°	856.30	63.634	.022	27°	1375.6	162.81	.083
10°	358.81	11.224	15° C.	10°	864.82	64.900	15° C.	10°	1384.4	164.86	.115
20°	367.17	11.753	T	20°	873.35	66.178	T	20°	1393.2	166.95	T
30°	375.54	12.294	E	30°	881.88	67.470	E	30°	1402.0	169.04	E
40°	383.91	12.847	.03	40°	890.41	68.774	.06	40°	1410.9	171.15	.10
50°	392.28	13.413	E	50°	898.95	70.091	E	50°	1419.7	173.27	E
8°	400.66	13.991	.007	18°	907.49	71.421	.028	28°	1428.6	175.41	.115
10°	409.03	14.582	15° C.	10°	916.03	72.764	15° C.	10°	1437.4	177.55	.147
20°	417.41	15.184	T	20°	924.58	74.119	T	20°	1446.3	179.72	T
30°	425.79	15.799	E	30°	933.13	75.488	E	30°	1455.1	181.89	E
40°	434.17	16.426	.03	40°	941.69	76.869	.06	40°	1464.0	184.08	.10
50°	442.55	17.065	E	50°	950.25	78.264	E	50°	1472.9	186.29	E
9°	450.93	17.717	.007	19°	958.81	79.671	.028	29°	1481.8	188.51	.115
10°	459.32	18.381	15° C.	10°	967.38	81.092	15° C.	10°	1490.7	190.74	.147
20°	467.71	19.058	T	20°	975.96	82.525	T	20°	1499.6	192.99	T
30°	476.10	19.746	E	30°	984.53	83.972	E	30°	1508.5	195.25	E
40°	484.49	20.447	.03	40°	993.12	85.431	.06	40°	1517.4	197.53	.10
50°	492.88	21.161	E	50°	1001.7	86.904	E	50°	1526.3	199.82	E
10°	501.28	21.887	.008	20°	1010.3	88.389	.034	30°	1535.3	202.12	.115
10°	509.68	22.624	15° C.	10°	1018.9	89.888	15° C.	10°	1544.2	204.44	.147
20°	518.08	23.375	T	20°	1027.5	91.399	T	20°	1553.1	206.77	T
30°	526.48	24.138	E	30°	1036.1	92.924	E	30°	1562.1	209.12	E
40°	534.89	24.913	.03	40°	1044.7	94.462	.06	40°	1571.0	211.48	.10
50°	543.29	25.700	E	50°	1053.3	96.013	E	50°	1580.0	213.86	E

T = R tan 1/2 I

E = R exsec 1/2 I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	387.4	+	51°	2732.9	618.4	+
10°	1598.0	218.7	5° C.	10°	2151.7	390.7	5° C.	10°	2743.1	622.8	5° C.
20°	1606.9	221.1	T	20°	2161.2	394.1	T	20°	2753.4	627.2	T
30°	1615.9	223.5	E	30°	2170.8	397.4	E	30°	2763.7	631.7	E
40°	1624.9	226.0	.13	40°	2180.3	400.8	.17	40°	2773.9	636.2	.21
50°	1633.9	228.4	E	50°	2189.9	404.2	E	50°	2784.2	640.7	E
32°	1643.0	230.9	.023	42°	2199.4	407.6	.037	52°	2794.0	645.2	.056
10°	1652.0	233.4	10° C.	10°	2209.0	411.1	10° C.	10°	2804.9	649.7	10° C.
20°	1661.0	235.9	T	20°	2218.6	414.5	T	20°	2815.2	654.3	T
30°	1670.0	238.4	E	30°	2228.1	418.0	E	30°	2825.6	658.8	E
40°	1679.1	241.0	.04	40°	2237.7	421.4	.05	40°	2835.9	663.4	.05
50°	1688.1	243.5	E	50°	2247.3	425.0	E	50°	2846.3	668.0	E
33°	1697.2	246.1	.046	43°	2257.0	428.5	.075	53°	2856.7	672.7	.075
10°	1706.3	248.7	10° C.	10°	2266.6	432.0	10° C.	10°	2867.1	677.3	10° C.
20°	1715.3	251.3	T	20°	2276.2	435.6	T	20°	2877.5	682.0	T
30°	1724.4	253.9	E	30°	2285.9	439.2	E	30°	2888.0	686.7	E
40°	1733.5	256.5	.06	40°	2295.6	442.8	.08	40°	2898.4	691.4	.08
50°	1742.6	259.1	E	50°	2305.2	446.4	E	50°	2908.9	696.1	E
34°	1751.7	261.8	.06	44°	2314.9	450.0	.08	54°	2919.4	700.9	.08
10°	1760.8	264.5	15° C.	10°	2324.6	453.6	15° C.	10°	2929.9	705.7	15° C.
20°	1770.0	267.2	T	20°	2334.3	457.3	T	20°	2940.4	710.5	T
30°	1779.1	269.9	E	30°	2344.1	461.0	E	30°	2951.0	715.3	E
40°	1788.2	272.6	.08	40°	2353.8	464.6	.10	40°	2961.5	720.1	.10
50°	1797.4	275.3	E	50°	2363.5	468.4	E	50°	2972.1	725.0	E
35°	1806.6	278.1	.08	45°	2373.3	472.1	.12	55°	2982.7	729.9	.12
10°	1815.7	280.8	15° C.	10°	2383.1	475.8	15° C.	10°	2993.3	734.8	15° C.
20°	1824.9	283.6	T	20°	2392.8	479.6	T	20°	3003.9	739.7	T
30°	1834.1	286.4	E	30°	2402.6	483.4	E	30°	3014.5	744.6	E
40°	1843.3	289.2	.10	40°	2412.4	487.2	.12	40°	3025.2	749.6	.12
50°	1852.5	292.0	E	50°	2422.3	491.0	E	50°	3035.8	754.6	E
36°	1861.7	294.9	.10	46°	2432.1	494.8	.14	56°	3046.5	759.6	.14
10°	1870.9	297.7	15° C.	10°	2441.9	498.7	15° C.	10°	3057.2	764.6	15° C.
20°	1880.1	300.6	T	20°	2451.8	502.5	T	20°	3067.9	769.7	T
30°	1889.4	303.5	E	30°	2461.7	506.4	E	30°	3078.7	774.7	E
40°	1898.6	306.4	.12	40°	2471.5	510.3	.14	40°	3089.4	779.8	.14
50°	1907.9	309.3	E	50°	2481.4	514.3	E	50°	3100.2	784.9	E
37°	1917.1	312.2	.12	47°	2491.3	518.2	.16	57°	3110.9	790.1	.16
10°	1926.4	315.2	15° C.	10°	2501.2	522.2	15° C.	10°	3121.7	795.2	15° C.
20°	1935.7	318.1	T	20°	2511.2	526.1	T	20°	3132.6	800.4	T
30°	1945.0	321.1	E	30°	2521.1	530.1	E	30°	3143.4	805.6	E
40°	1954.3	324.1	.14	40°	2531.1	534.2	.16	40°	3154.2	810.9	.16
50°	1963.6	327.1	E	50°	2541.0	538.2	E	50°	3165.1	816.1	E
38°	1972.9	330.2	.14	48°	2551.0	542.2	.18	58°	3176.0	821.4	.18
10°	1982.2	333.2	15° C.	10°	2561.0	546.3	15° C.	10°	3186.9	826.7	15° C.
20°	1991.5	336.3	T	20°	2571.0	550.4	T	20°	3197.8	832.0	T
30°	2000.9	339.3									

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=70°	I	T	E	I=80°	I	T	E	I=90°
61°	3375.0	920.2	+	71°	4086.9	1308.2	+	81°	4893.6	1805.3	+
10'	3386.3	925.9		10'	4099.5	1315.6		10'	4908.0	1814.7	
20'	3397.5	931.6	5° C.	20'	4112.1	1322.9	5° C.	20'	4922.5	1824.1	5° C.
30'	3408.8	937.3	T	30'	4124.8	1330.3	T	30'	4937.0	1833.6	T
40'	3420.1	943.1	.25	40'	4137.4	1337.7	.30	40'	4951.5	1843.1	.36
50'	3431.4	948.9	E	50'	4150.1	1345.1	E	50'	4966.1	1852.6	E
62°	3442.7	954.8	.080	72°	4162.8	1352.6	.110	82°	4980.7	1862.2	.149
10'	3454.1	960.6		10'	4175.6	1360.1		10'	4995.4	1871.8	
20'	3465.4	966.5		20'	4188.5	1367.6		20'	5010.0	1881.5	
30'	3476.8	972.4		30'	4201.2	1375.2		30'	5024.8	1891.2	
40'	3488.3	978.3		40'	4214.0	1382.8		40'	5039.5	1900.9	
50'	3499.7	984.3		50'	4226.8	1390.4		50'	5054.3	1910.7	
63°	3511.1	990.2	10° C.	73°	4239.7	1398.0	10° C.	83°	5069.2	1920.5	10° C.
10'	3522.6	996.2	T	10'	4252.6	1405.7	T	10'	5084.0	1930.4	T
20'	3534.1	1002.3		20'	4265.6	1413.5		20'	5099.0	1940.3	
30'	3545.6	1008.3	.51	30'	4278.5	1421.2	.61	30'	5113.9	1950.3	.72
40'	3557.2	1014.4	E	40'	4291.5	1429.0	E	40'	5128.9	1960.2	E
50'	3568.7	1020.5	.159	50'	4304.6	1436.8	.220	50'	5143.9	1970.3	.299
64°	3580.3	1026.6		74°	4317.6	1444.6		84°	5159.0	1980.4	
10'	3591.9	1032.8		10'	4330.7	1452.5		10'	5174.1	1990.5	
20'	3603.5	1039.0		20'	4343.8	1460.4		20'	5189.3	2000.6	
30'	3615.1	1045.2		30'	4356.9	1468.4		30'	5204.4	2010.8	
40'	3626.8	1051.4		40'	4370.1	1476.4		40'	5219.7	2021.1	
50'	3638.5	1057.7	15° C.	50'	4383.3	1484.4	15° C.	50'	5234.9	2031.4	15° C.
65°	3650.2	1063.9	T	75°	4396.5	1492.4	T	85°	5250.3	2041.7	T
10'	3661.9	1070.2	.76	10'	4409.8	1500.5	.91	10'	5265.6	2052.1	1.09
20'	3673.7	1076.6	E	20'	4423.1	1508.6	E	20'	5281.0	2062.5	E
30'	3685.5	1082.9		30'	4436.4	1516.7		30'	5296.4	2073.0	
40'	3697.2	1089.3	.240	40'	4449.7	1524.9	.332	40'	5311.9	2083.5	.450
50'	3709.0	1095.7		50'	4463.1	1533.1		50'	5327.4	2094.1	
66°	3720.9	1102.2		76°	4476.5	1541.4		86°	5343.0	2104.7	
10'	3732.7	1108.6		10'	4489.9	1549.7		10'	5358.6	2115.3	
20'	3744.6	1115.1		20'	4503.4	1558.0		20'	5374.2	2126.0	
30'	3756.5	1121.7		30'	4516.9	1566.3		30'	5389.9	2136.7	
40'	3768.5	1128.2	20° C.	40'	4530.4	1574.7	20° C.	40'	5405.6	2147.5	20° C.
50'	3780.4	1134.8	T	50'	4544.0	1583.1	T	50'	5421.4	2158.4	T
67°	3792.4	1141.4	1.02	77°	4557.6	1591.6	1.22	87°	5437.2	2169.2	1.45
10'	3804.4	1148.0	E	10'	4571.2	1600.1	E	10'	5453.1	2180.2	E
20'	3816.4	1154.7	.321	20'	4584.8	1608.6	.445	20'	5469.0	2191.1	.603
30'	3828.4	1161.3		30'	4598.5	1617.1		30'	5484.9	2202.2	
40'	3840.5	1168.1		40'	4612.2	1625.7		40'	5500.9	2213.2	
50'	3852.6	1174.8		50'	4626.0	1634.4		50'	5517.0	2224.3	
68°	3864.7	1181.6		78°	4639.8	1643.0		88°	5533.1	2235.5	
10'	3876.8	1188.4		10'	4653.6	1651.7		10'	5549.2	2246.7	
20'	3889.0	1195.2	25° C.	20'	4667.4	1660.5	25° C.	20'	5565.4	2258.0	25° C.
30'	3901.2	1202.0	T	30'	4681.3	1669.2	T	30'	5581.6	2269.3	T
40'	3913.4	1208.9	1.28	40'	4695.2	1678.1	1.53	40'	5597.8	2280.6	1.83
50'	3925.6	1215.8	E	50'	4709.2	1686.9	E	50'	5614.2	2292.0	E
69°	3937.9	1222.7	.403	79°	4723.2	1695.8	.558	89°	5630.5	2303.5	.756
10'	3950.2	1229.7		10'	4737.2	1704.7		10'	5646.9	2315.0	
20'	3962.5	1236.7		20'	4751.2	1713.7		20'	5663.4	2326.6	
30'	3974.8	1243.7		30'	4765.3	1722.7		30'	5679.9	2338.2	
40'	3987.2	1250.8		40'	4779.4	1731.7		40'	5696.4	2349.8	
50'	3999.5	1257.9		50'	4793.6	1740.8		50'	5713.0	2361.5	
70°	4011.9	1265.0	30° C.	80°	4807.7	1749.9	30° C.	90°	5729.7	2373.3	30° C.
10'	4024.4	1272.1	T	10'	4822.0	1759.0	T	10'	5746.3	2385.1	T
20'	4036.8	1279.3	1.54	20'	4836.2	1768.2	1.84	20'	5763.1	2397.0	2.20
30'	4049.3	1286.5	E	30'	4850.5	1777.4	E	30'	5779.9	2408.9	E
40'	4061.8	1293.6		40'	4864.8	1786.6		40'	5796.7	2420.9	
50'	4074.4	1300.9	.485	50'	4879.2	1796.0	.671	50'	5813.6	2432.9	.910

T = R tan ½ I

E = R exsec ½ I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=100°	I	T	E	I=110°	I	T	E	I=120°
91°	5830.5	2444.9	+	101°	6950.6	3278.1	+	111°	8336.7	4386.1	+
10'	5847.5	2457.1		10'	6971.3	3294.1		10'	8362.7	4407.6	
20'	5864.6	2469.3	5° C.	20'	6992.0	3310.1	5° C.	20'	8388.9	4429.2	5° C.
30'	5881.7	2481.5	T	30'	7012.7	3326.1	T	30'	8415.1	4450.9	T
40'	5898.8	2493.8	.43	40'	7033.6	3342.3	.51	40'	8441.5	4472.7	.62
50'	5916.0	2506.1	E	50'	7054.5	3358.5	E	50'	8468.0	4494.6	E
92°	5933.2	2518.5	.200	102°	7075.5	3374.9	.268	112°	8494.6	4516.6	.360
10'	5950.5	2531.0		10'	7096.6	3391.2		10'	8521.3	4538.8	
20'	5967.9	2543.5		20'	7117.8	3407.7		20'	8548.1	4561.1	
30'	5985.3	2556.0		30'	7139.0	3424.3		30'	8575.0	4583.4	
40'	6002.7	2568.6		40'	7160.3	3440.9		40'	8602.1	4606.0	
50'	6020.2	2581.3		50'	7181.7	3457.6		50'	8629.3	4628.6	
93°	6037.8	2594.0	10° C.	103°	7203.2	3474.4	10° C.	113°	8656.6	4651.3	10° C.
10'	6055.4	2606.8	T	10'	7224.7	3491.3	T	10'	8684.0	4674.2	T
20'	6073.1	2619.7	.86	20'	7246.3	3508.2	.103	20'	8711.5	4697.2	1.25
30'	6090.8	2632.6	E	30'	7268.0	3525.2	F	30'	8739.2	4720.3	E
40'	6108.6	2645.5	.401	40'	7289.8	3542.4	.536	40'	8767.0	4743.6	.721
50'	6126.4	2658.5		50'	7311.7	3559.6		50'	8794.9	4766.9	
94°	6144.3	2671.6		104°	7333.6	3576.8		114°	8822.9	4790.4	
10'	6162.2	2684.7		10'	7355.6	3594.2		10'	8851.0	4814.1	
20'	6180.2	2697.9		20'	7377.8	3611.7		20'	8879.3	4837.8	
30'	6198.3	2711.2		30'	7399.9	3629.2		30'	8907.7	4861.7	
40'	6216.4	2724.5		40'	7422.2	3646.8		40'	8936.3	4885.7	
50'	6234.6	2737.9	15° C.	50'	7444.6	3664.5	15° C.	50'	8965.0	4909.9	15° C.
95°	6252.8	2751.3	T	105°	7467.0	3682.3	T	115°	8993.8	4934.1	T
10'	6271.1	2764.8	1.30	10'	7489.6	3700.2	1.56	10'	9022.7	4958.6	1.93
20'	6289.4	2778.3	E	20'	7512.2	3718.2	E	20'	9051.7	4983.1	E
30'	6307.9	2792.0	.604	30'	7534.9	3736.2	.806	30'	9080.9	5007.8	1.09
40'	6326.3	2805.6		40'	7557.7	3754.4		40'	9110.3	5032.6	
50'	6344.8	2819.4		50'	7580.5	3772.6		50'	9139.8	5057.6	
96°	6363.4	2833.2		106°	7603.5	3791.0		116°	9169.4	5082.7	
10'	6382.1	2847.0		10'	7626.6	3809.4		10'	9199.1	5107.9	
20'	6400.8	2861.0		20'	7649.7	3827.9		20'	9229.0	5133.3	
30'	6419.5	2875.0		30'	7672.9	3846.5		30'	9259.0	5158.8	
40'	6438.4	2889.0	20° C.	40'	7696.3	3865.2	20° C.	40'	9289.2	5184.5	20° C.
50'	6457.3	2903.1	T	50'	7719.7	3884.0	T	50'	9319.5	5210.3	T
97°	6476.2	2917.3	1.74	107°	7743.2	3902.9	2.08	117°	9349.9	5236.2	2.52
10'	6495.2	2931.6	E	10'	7766.8	3921.9	E	10'	9380.5	5262.3	E
20'	6514.3	2945.9	.809	20'	7790.5	3940.9	1.08	20'	9411.3	5288.6	1.46
30'	6533.4	2960.3		30'	7814.3	3960.1		30'	9442.2	5315.0	
40'	6552.6	2974.7		40'	7838.1	3979.4		40'	9473.2	5341.5	
50'	6571.9	2989.2		50'	7862.1	3998.7		50'	9504.4	5368.2	
98°	6591.2	3003.8		108°	7886.2	4018.2		118°	9535.7	5395.1	
10'	6610.6	3018.4		10'	7910.4	4037.8		10'	9567.2	5422.1	
20'	6630.1	3033.1	25° C.	20'	7934.6	4057.4	25° C.	20'	9598.9	5449.2	25° C.
30'	6649.6	3047.9	T	30'	7959.0	4077.2	T	30'	9630.7	5476.5	T
40'	6669.2	3062.8	2.18	40'	7983.5	4097.1	2.61	40'	9662.6	5504.0	3.16
50'	6688.8	3077.7	E	50'	8008.0	4117.0	E	50'	9694.7	5531.7	E
99°	6708.6	3092.7	1.02</								

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord and multiply by length of chord.

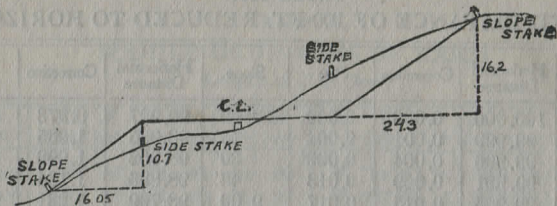
TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise	Slope	Horizontal Distance	Correction	Rise
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.153
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

For each foot take one one-hundredth of each reading.

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 10"	.50833	40' 30"	.67500	50' 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
2 00	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
3 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

348.48
 125) 43560
 375

 606
 500

 1060
 10 00

600
 500

 1000
 11413.73
 9513.56

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER

**COURT HOUSE
 CHARDON, O.
 PHONE 250-X**

TABLE OF INCHES REDUCED TO DECIMALS OF A FOOT.

Inch	Dec.	Inch	Dec.	Inch	Dec.	Inch	Dec.	Inch	Dec.	Inch	Dec.
1	.0625	11	.8750	21	.8375	31	.8438	41	.8490	51	.8542
2	.1250	12	.9000	22	.8625	32	.8594	42	.8646	52	.8698
3	.1875	13	.9125	23	.8750	33	.8750	43	.8750	53	.8750
4	.2500	14	.9250	24	.8875	34	.8854	44	.8854	54	.8854
5	.3125	15	.9375	25	.9000	35	.8906	45	.8906	55	.8906
6	.3750	16	.9500	26	.9125	36	.8958	46	.8958	56	.8958
7	.4375	17	.9625	27	.9250	37	.9010	47	.9010	57	.9010
8	.5000	18	.9750	28	.9375	38	.9063	48	.9063	58	.9063
9	.5625	19	.9875	29	.9500	39	.9115	49	.9115	59	.9115
10	.6250	20	.1.0000	30	.9625	40	.9167	50	.9167	60	.9167
11	.6875										
12	.7500										
13	.8125										
14	.8750										
15	.9375										
16	.1.0000										

B. K. ELLIOTT COMPANY, PITTSBURG, PA.
 DRAWING MATERIALS AND SURVEYING INSTRUMENTS

Handwritten calculations and diagrams on the left page of the notebook. The page contains several arithmetic problems, some with multiple steps, and several geometric diagrams. The diagrams appear to be surveying plots or triangles with various measurements and angles. Some of the numbers and results include:

- 1264
- 1288
- 1272
- 1236
- 13383.42
- 11413.73
- 1969.67
- 5.60
- 3920
- 3911
- 3690
- 4283
- 17274.4
- 16355.55
- 918.85
- 9.24
- 1221
- 122
- 10195
- 3976
- 1908
- 4.77
- 3339
- 95.500
- 94.2
- 1300
- 1250
- 18198
- 17274
- 9.24

There are also several small diagrams showing triangles and lines with various labels and measurements, possibly representing land surveying data.

